

# NACA

## RESEARCH MEMORANDUM

EFFECTS OF LEADING-EDGE CHORD EXTENSIONS AND AN ALL-MOVABLE HORIZONTAL TAIL ON THE AERODYNAMIC CHARAC-TERISTICS OF A WING-BODY COMBINATION EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 MOUNTED IN A HIGH POSITION AT SUB-SONIC AND SUPERSONIC SPEEDS

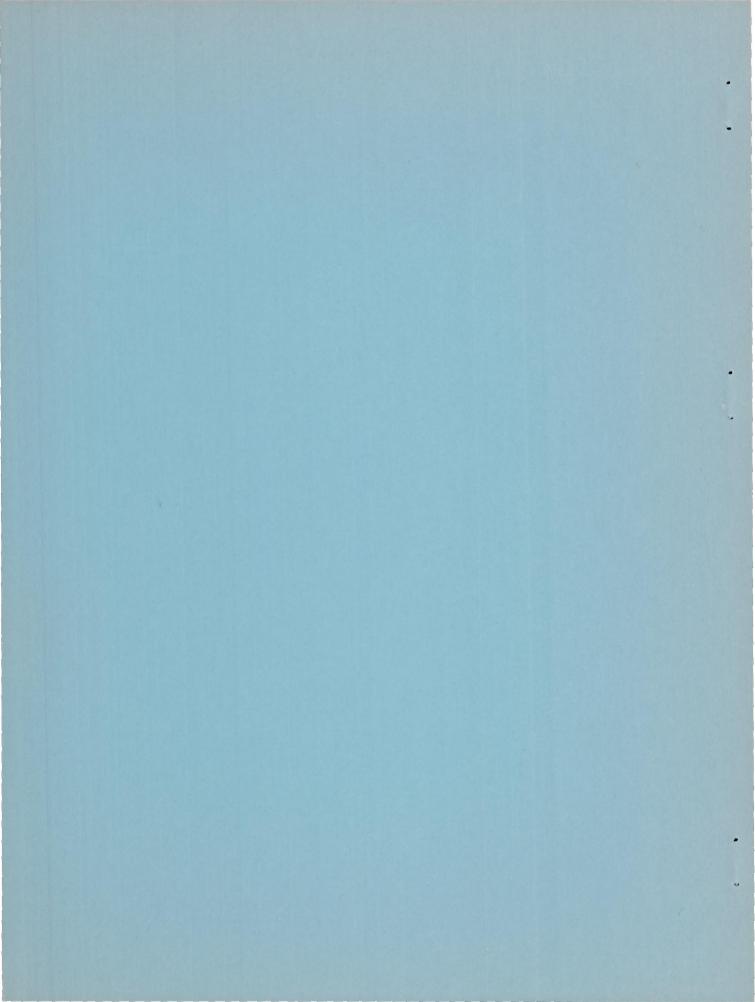
By Benton E. Wetzel and Frank A. Pfyl

EFFECTIVE DATE: OCTOBER

# By Benton E. Wetzel and Frank A. Pfyl Ames Aeronautical Laboratory Moffett Field, Calif. CLASSIFIED DOCUMENT This material contains information affecting the National Defense of the United States within the meaning of the espionage laws, Title 18, U.S.C., Secs. 783 and 794, the transmission or revelation of which in any manner to an unauthorized person is prohibited by law. NATIONAL ADVISORY COMMITTEES TOOR AEROCALAUTICE FOR AERONAUTICS

WASHINGTON

January 6, 1954



#### NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

#### RESEARCH MEMORANDUM

EFFECTS OF LEADING-EDGE CHORD EXTENSIONS AND AN ALLMOVABLE HORIZONTAL TAIL ON THE AERODYNAMIC CHARACTERISTICS OF A WING-BODY COMBINATION EMPLOYING
A TRIANGULAR WING OF ASPECT RATIO 3
MOUNTED IN A HIGH POSITION AT SUBSONIC AND SUPERSONIC SPEEDS

By Benton E. Wetzel and Frank A. Pfyl

#### SUMMARY

The results of an experimental investigation of the effect of leading-edge chord extensions on the aerodynamic characteristics of a wing-body-tail combination employing a 3-percent-thick triangular wing of aspect ratio 3 in conjunction with an unswept, all-movable, horizontal tail located below the wing-chord plane are presented. Lift, drag, pitching moment, and hinge moment were measured at Mach numbers varying from 0.6 to 0.9 and from 1.2 to 1.9, at a Reynolds number of 3.8 million. The angle of attack was varied from -4° to +17° at constant horizontal-tail deflections varying from +4° to -24°. Data are also presented for the model without the horizontal tail.

The wing-body-tail combination was tested with 13.35-percent-chord, leading-edge chord extensions on the outer 50 percent of the wing semispan in an effort to improve the undesirable static longitudinal stability characteristics of the triangular wing at moderate-to-high lift coefficients at subsonic speeds. To improve, also, the subsonic lift and drag characteristics, the chord extensions were drooped 3°.

Comparisons of the results obtained for the wing-body-tail combination having chord extensions with those for the combination without chord extensions showed that the extensions improved the lift, drag, and pitching-moment characteristics at moderate-to-high lift coefficients at subsonic speeds and had small effect on those characteristics at supersonic speeds. Static longitudinal instability, which occurred in a range of moderate lift coefficients at Mach numbers of 0.6 and 0.8 for the model without chord extensions, was either eliminated (M = 0.8) or delayed to higher lift coefficients (M = 0.6). Improved variations of lift with angle of attack at the aforementioned Mach numbers and

increased maximum lift-drag ratios at Mach numbers from 0.6 to 1.3 were realized from the addition of chord extensions. Essentially no changes in the hinge-moment characteristics were brought about at either subsonic or supersonic speeds by the addition of chord extensions.

#### INTRODUCTION

As part of a program devoted to the investigation of components of interceptor-type supersonic aircraft, a wing-body-tail combination employing a 3-percent-thick triangular wing of aspect ratio 3 and an all-movable horizontal tail was tested in the Ames 6- by 6-foot supersonic wind tunnel. The wing was mounted high on the body, and the tail was below the wing-chord plane. Previous tests of the wing-body combination (ref. 1) showed losses in stability at moderate-to-high lift coefficients at subsonic speeds. Tests of models similar to the present one (ref. 2) have indicated that such variations in stability might be avoided or minimized by locating the horizontal tail in certain positions below the extended chord plane of the wing; however, when the tail was added to the present model, the instability still persisted, and the presence of the tail had little influence upon stability variations. Therefore, the possibility of improving the stability by modifying the wing so as to reduce the center-of-pressure movement was investigated.

This center-of-pressure movement has been shown by previous tests of thin triangular wings to result from flow separation at the wing tips. This flow separation is believed to be accompanied by separation vortices (ref. 3) generated on the upper surface of the wing, which could have an adverse effect on the stability. Research on sweptback wings (e.g., ref. 4) has shown that improvement of the characteristics of such wings can be obtained through the use of leading-edge chord extensions, which serve either to eliminate or to reduce separation or vortex-type flow over the tip sections. An effort was made to improve the longitudinal stability characteristics of the present model through the addition of such devices. The chord extensions were drooped a small amount in order to obtain improved subsonic drag characteristics, such as were reported in reference 4.

The present paper is devoted primarily to the comparison of the lift, drag, and pitching-moment characteristics of the wing-body-tail combination with and without the leading-edge chord extensions and to the presentation of the control-surface characteristics of the combination with chord extensions.

#### SYMBOLS

b wing span, in.

CD drag coefficient, drag

hinge-moment coefficient,  $\frac{\text{hinge moment}}{\text{qS}_{\text{t}}\bar{c}_{\text{t}}}$ , measured about an axis at 30 percent of the chord of the horizontal tail

C<sub>L</sub> lift coefficient, lift qS

Cm pitching-moment coefficient, pitching moment, referred to a qSc

horizontal axis through the point on the body axis corresponding to 35-percent mean aerodynamic chord of the wing

c local wing chord of the wing without chord extensions, in.

ct local chord of the horizontal tail, in.

mean aerodynamic chord of the wing,  $\frac{\int_0^{b/2} c^2 dy}{\int_0^{b/2} c dy}$ , in.

ct mean aerodynamic chord of horizontal tail, in.

 $\left(\frac{L}{D}\right)_{max}$  maximum lift-drag ratio

M free-stream Mach number

q free-stream dynamic pressure, lb/sq in.

R Reynolds number based on the mean aerodynamic chord of the wing

wing area, formed by extending the leading and trailing edges to the plane of symmetry, sq in.

(The additional area provided by the leading-edge chord extensions has not been included.)

St area of horizontal tail, formed by extending the leading and trailing edges to the plane of symmetry, sq in.

- y spanwise distance from plane of symmetry, in.
- α angle of attack of body axis, deg
- angle of horizontal-tail deflection, positive for trailing edge down, deg
- δ<sub>n</sub> nominal (no load) horizontal-tail deflection, deg

#### APPARATUS AND MODEL

The experimental investigation was conducted in the Ames 6- by 6-foot supersonic wind tunnel, which is a closed-section, variable-pressure-type tunnel with a Mach number range from 0.6 to 0.9 and from 1.2 to 1.9. A complete description of this facility has been published in reference 5. In this wind tunnel, models are sting-mounted, and over-all forces are measured with an internal electrical strain-gage balance. The model was also equipped with an electrical strain gage which measured the hinge moments on the horizontal tail.

The model consisted of a triangular wing, an all-movable horizontal tail, two vertical fins, and a body. The wing was mounted in a high position on the body, had an aspect ratio of 3, and was composed of NACA 0003-63 airfoil sections in streamwise planes. During a portion of the investigation, the wing was equipped with 13.35-percent-chord, leading-edge chord extensions over the outer 50-percent semispan of the wing, as shown in figure 1. The extensions had the same ordinates as the corresponding wing airfoil sections, with smooth fairings providing the transitions between the extensions and the wing. The chord extensions were drooped 3° with respect to the chord line.

The horizontal tail, which was mounted in a midposition on the body, was pivoted at the 30-percent-chord point and had a taper ratio of 0.4 and an aspect ratio of 5. The airfoil section in a streamwise plane was biconvex, with a maximum thickness-chord ratio of 3 percent at 30-percent chord. The tail was supported at the tips by the two vertical fins rigidly attached to the wing at the 50-percent-semispan station. These fins were of aspect ratio 2.08 and had a 3-percent-thick biconvex section in a streamwise plane. The wing and tail surfaces were of solid steel construction.

The body was the same as that described in reference 1 for use in conjunction with the wings positioned off the body axis. It had a fineness ratio of 9.86. A photograph of the complete model is shown in figure 2.

#### TEST AND PROCEDURE

#### Range of Test Variables

Lift, drag, pitching-moment, and hinge-moment characteristics of the model were investigated for a range of Mach numbers varying from 0.6 to 0.9 and from 1.2 to 1.9 at nominal angles of attack varying from -4° to a maximum of +17°. The model with horizontal tail installed was tested at horizontal-tail deflections varying from +4° to -24°, generally in 4° increments. The data were obtained at a Reynolds number of 3.8 million, based on the wing mean aerodynamic chord.

#### Reduction of Data

The test data have been reduced to standard NACA coefficient form. The pitching moments were calculated about a horizontal axis through the point on the body axis corresponding to 35 percent of the mean aerodynamic chord. Factors which affect the accuracy of these data are discussed in the following paragraphs.

Tunnel-wall interference. - Corrections to the subsonic results for the induced effects of the wind-tunnel walls resulting from lift on the model were made according to the methods of reference 6. The numerical values of these corrections, which were added to the uncorrected data, are:

$$\Delta \alpha = 0.5517 C_{L}$$

$$\Delta C_{\rm D} = 0.0096 \, C_{\rm L}^2$$

The correction to the pitching-moment coefficient was negligible.

Constriction of the flow at subsonic speeds was taken into account in the manner outlined in reference 7. At a Mach number of 0.9, the correction amounted to a 2-percent increase in the Mach number over that determined from a calibration of the wind tunnel without a model in place.

For the tests at supersonic speeds, the reflection from the tunnel wall of the Mach wave originating at the nose of the body crossed the horizontal tail only at a Mach number of 1.2. It is believed that the resulting interference effects were small, and no corrections were made for tunnel-wall effects.

Stream variations. - Tests at subsonic speeds in the 6- by 6-foot supersonic wind tunnel have indicated a small stream curvature and an

inclination in the pitch plane of the model. No correction for this stream curvature has been made. A survey of the airstream at supersonic speeds, reported in reference 5, has shown curvature and inclination only in the yaw plane of the model. The effects of this curvature on the measured aerodynamic characteristics of the model are not known but are believed to be small, as they were shown to be in the case of reference 8.

Surveys at both subsonic and supersonic speeds indicated that there is a static-pressure variation of sufficient magnitude in the wind-tunnel test section to affect the drag measurements. Corrections were added to the measured drag coefficients, therefore, to account for the longitudinal force resulting from the static-pressure variation. The maximum corrections were +0.0007 at a Mach number of 0.9 and -0.0008 at a Mach number of 1.3.

Support interference. At subsonic speeds, the effects of support interference on the aerodynamic characteristics of the model are not known. It is believed that such effects consist primarily of a change in the pressure at the base of the model. In an effort to correct at least partially for this support interference, the base pressure was measured and the drag data adjusted to correspond to a base pressure equal to the static pressure of the free stream.

At supersonic speeds, the interference of the sting on a body of a body-sting combination similar to that of the present model is shown by reference 9 to be confined to a change in base pressure. The abovementioned adjustment of the drag for pressure at the base of the model, therefore, was applied also to the data obtained at supersonic speeds.

#### Precision

The uncertainties involved in determining dynamic pressure and in measuring forces with the strain-gage balance are described fully in reference 10. The following table lists the maximum uncertainty introduced into each corrected coefficient by the known uncertainties in the measurements:

Quantity	Uncertainty
Lift coefficient	±0.002
Drag coefficient	±0.0010
Pitching-moment coefficient	±0.002
Hinge-moment coefficient	±0.005
Mach number	±0.01
Reynolds number	$\pm 0.03 \times 10^{6}$
Angle of attack	±0.10°
Horizontal-tail deflection	±0.25°

#### RESULTS

The experimental results obtained during the investigation are presented in tables I and II for the complete range of test variables. The results for the wing-body and the wing-body-tail combinations without leading-edge chord extensions are presented in table I, those for the combinations with chord extensions in table II. For the purpose of analysis, a portion of these data is presented in graphical form.

The effect of the chord extensions on the variation of pitchingmoment coefficient with lift coefficient for the model with the
horizontal tail removed (but with the vertical fins attached to the
wing) is shown in figure 3 for several subsonic and supersonic Mach
numbers. The effect of the chord extensions on the pitching-moment,
lift, and drag characteristics of the wing-body-tail combination for a
nominal horizontal-tail deflection of zero is shown in figure 4 for the
same Mach numbers.

In order to permit a more detailed evaluation of the effect of the chord extensions on the drag characteristics, the variation with Mach number of the drag coefficient at various lift coefficients and the variation with Mach number of the maximum lift-drag ratio are presented in figures 5 and 6, respectively.

The variation of the pitching-moment coefficient with horizontal-tail deflection is shown in figure 7. The variations of hinge-moment coefficient with horizontal-tail deflection and with angle of attack are presented in figures 8 and 9 for the model with chord extensions. A study of the data for the combinations with and without chord extensions showed essentially no difference in the control-effectiveness and hinge-moment characteristics as a result of adding the chord extensions. Therefore, only the results for the wing-body-tail combination with chord extensions are presented graphically. The data presented in these figures have been limited to Mach numbers of 0.6, 0.9, 1.3, and 1.9, since these were considered sufficient to show the variations through the Mach number range. Horizontal-tail deflections noted in figure 8 are nominal settings of the tail surfaces. The actual deflection angles, which changed slightly under aerodynamic load, can be obtained from table II.

#### DISCUSSION

In the section to follow, two features of the data will be discussed. First, the effects of the chord extensions on the basic aerodynamic characteristics of the wing-body and the wing-body-tail

combinations will be considered. A brief discussion of the controlsurface characteristics will follow.

#### Basic Characteristics

Pitching moment. - As was noted previously, some loss in stability was shown to exist for the wing-body combination at moderate-to-high lift coefficients at subsonic speeds during a previous investigation (ref. 1). With the center of gravity at 35-percent mean aerodynamic chord, the loss in stability was of such magnitude as to result in an unstable variation of pitching-moment coefficient at Mach numbers of 0.6 and 0.8 for the model with the horizontal tail removed. (See fig. 3.) With the horizontal tail added to the wing-body combination (fig. 4(a)), the unstable variation at these subsonic speeds still existed. That the longitudinal instability of the wing-body combination was due largely to the instability of the wing-body combination can be determined from a comparison of figures 3 and 4(a). As indicated in figure 3, addition of the chord extensions improved the pitching-moment characteristics of the wing-body combination, the instability being either eliminated (M = 0.8) or delayed to a higher lift coefficient (M = 0.6). A similar improvement occurred for the wing-body-tail combination (fig. 4(a)). It should be noted that addition of the chord extensions had little effect on the tail contribution to the stability. At supersonic speeds, the chord extensions had only small effect on the pitching-moment characteristics.

Lift. The results for the wing-body-tail combination without chord extensions (fig. 4(b)) showed a range of angle of attack near 8° at Mach numbers of 0.6 and 0.8 in which the lift-curve slope was considerably less than at other angles of attack. This decrease in lift-curve slope appeared initially at about the same lift coefficient as the onset of pitching-moment instability. With chord extensions installed, the lift was maintained up to angles of attack of the order of 16°. The improvement in the lift characteristics is believed to be due primarily to the ability of the chord extensions to improve the flow over the wing tips. At supersonic speeds, the chord extensions had little effect on the lift characteristics. The slight increase in lift-curve slope shown in figure 4(b) may have been due to the increased area provided by the chord extensions.

Drag. - The drag results, presented in figures 4(c) and 5, indicate that the addition of the chord extensions increased slightly the minimum drag coefficient throughout the speed range investigated, although this increase was of the same order of magnitude as the maximum uncertainty of measurement. On the other hand, at lift coefficients greater than 0.2, the chord extensions reduced significantly the drag coefficients at subsonic speeds and at a Mach number of 1.3. The reduction in drag at

these lift coefficients is believed to be due, primarily, to the small amount of camber which resulted from the drooping of the chord extensions. Drooping the leading edge tends to maintain high lifting pressures on that portion of the wing and to provide a component of force in the thrust direction. At Mach numbers greater than 1.5, the beneficial effect of the chord extensions on the drag no longer existed. At the higher lift coefficients, the apparent benefit of the chord extensions shown at these Mach numbers can be attributed to the increased area provided by the chord extensions.

The effect of the chord extensions on the maximum lift-drag ratio is shown in figure 6. At a Mach number of 0.6 a large increase in (L/D) was realized, the improvement decreasing with increasing Mach number. In the supersonic speed range at Mach numbers of 1.5 and above, decreased lift-drag ratios were incurred with the chord extensions installed.

#### Control-Surface Characteristics

The following section is devoted to a discussion of the controlsurface characteristics of the tail when used in conjunction with the wing-body combination with chord extensions. As pointed out in Results, a study of the data for the models with and without chord extensions showed essentially no difference in the control-effectiveness and hinge-moment characteristics. Thus, statements made in the following discussion also apply to the characteristics of the tail when used with the wing-body combination without chord extensions.

Control effectiveness .- Increasing control effectiveness with increasing Mach number was indicated for the subsonic speed range, as shown in figure 7. The variation of pitching-moment coefficient with horizontal-tail deflection was linear throughout only a moderate range of deflection angles in this speed range. However, for an airplane with its center of gravity at 35 percent of the mean aerodynamic chord, this moderate range is sufficient to provide static longitudinal balance throughout the range of lift coefficients investigated. A large decrease in the effectiveness of the horizontal tail occurred as the Mach number was increased from subsonic to supersonic speed. At supersonic speeds, the variation of pitching moment with angle of deflection was linear up to fairly large negative angles, the control effectiveness decreasing with increasing Mach number.

Hinge-moment coefficient .- As noted above, static longitudinal balance could be obtained at subsonic speeds with small deflection of the control surfaces. As shown in figures 8 and 9, the variations of hinge-moment coefficient with angle of attack and with tail deflection were small throughout the range of deflection angles required for balance. As a result, the control forces required to deflect the horizontal-tail surfaces at subsonic speeds would be expected to be small. If, however, the center-of-gravity position were moved forward so that larger deflection angles were necessary for balance, larger variation of the hinge-moment coefficient with deflection angle would be encountered and larger control forces would be required.

At supersonic speeds, the magnitude of the variations of hinge-moment coefficient with angle of attack and with tail deflection increased greatly. As a result, large control forces would be expected to be required in this speed range. For example, if one considered the present wing-body-tail combination to be a 1/12-scale model of an air-plane with a wing loading of 45 pounds per square foot, the control moment at a Mach number of 1.5 would be of the order of 30 times that at a Mach number of 0.6 for level flight at an altitude of 30,000 feet.

#### CONCLUSIONS

Experimental wind-tunnel results for a wing-body-tail combination employing a 3-percent-thick triangular wing of aspect ratio 3 in conjunction with an unswept, all-movable horizontal tail show that the aerodynamic characteristics were improved at moderate-to-high lift coefficients at subsonic speeds and only slightly changed at supersonic speeds, due to the addition of leading-edge chord extensions to the wing. The results of the wind-tunnel investigation are given below.

Pitching moment.— High-lift instability which occurred at subsonic speeds at Mach numbers of 0.6 and 0.8 was either eliminated (M = 0.8) or delayed to higher lift coefficients (M = 0.6) through the addition of chord extensions. Only a small effect at supersonic Mach numbers resulted from the addition of chord extensions.

Lift. The addition of chord extensions eliminated undesirable lift characteristics at subsonic speeds and had little effect on the lift at supersonic speeds. Whereas the variation of lift coefficient with angle of attack for the wing-body-tail combination without chord extensions decreased rapidly at an angle of attack of about 8° at Mach numbers of 0.6 and 0.8, the variation for the combination with chord extensions had no inflection and lift was maintained up to angles of about 16°.

<u>Drag.-</u> The minimum drag was increased slightly throughout the Mach number range with the addition of chord extensions. At subsonic speeds, the drag due to lift was reduced, and the maximum lift-drag ratios were, in consequence, increased. The greatest increase in  $(L/D)_{max}$  was obtained at M = 0.6, the improvement decreasing with Mach number. At supersonic Mach numbers of 1.5 and greater, no improvement in drag due to lift was realized through the addition of chord extensions. Maximum

lift-drag ratios obtained in this Mach number range were, as a result, decreased slightly.

Control effectiveness. The control effectiveness of the horizontal tail was essentially unchanged by the addition of chord extensions. At subsonic speeds the effectiveness increased with increasing Mach number. A large decrease in effectiveness occurred as the Mach number was increased from subsonic to supersonic speed. At supersonic speeds the effectiveness decreased with increasing Mach number.

Hinge moment. - Essentially no changes in the hinge-moment characteristics of the horizontal tail occurred due to the addition of chord extensions. The variation of the hinge-moment coefficient with angle of attack and with horizontal-tail deflection was such that the control forces required to deflect the horizontal tail would be much larger at supersonic speeds than at subsonic speeds.

Ames Aeronautical Laboratory
National Advisory Committee for Aeronautics
Moffett Field, Calif., Oct. 14, 1953

#### REFERENCES

- 1. Heitmeyer, John C.: Effect of Vertical Position of the Wing on the on the Aerodynamic Characteristics of Three Wing-Body Combinations.

  NACA RM A52L15a, 1953.
- 2. Mitchell, Jesse L.: The Static and Dynamic Longitudinal Stability Characteristics of Some Supersonic Aircraft Configurations. NACA RM L52AlOa, 1952.
- 3. Anderson, Adrien E.: Chordwise and Spanwise Loadings Measured at Low Speed on Large Triangular Wings. NACA RM A9B17, 1949.
- 4. West, F. E., Jr., Liner, George, and Martz, Gladys S.: Effect of Leading-Edge Chord-Extensions on the Aerodynamic Characteristics of a 45° Sweptback Wing-Fuselage Combination at Mach Numbers of 0.40 to 1.03. NACA RM L53B02, 1953.
- 5. Frick, Charles W., and Olson, Robert N.: Flow Studies in the Asymmetric Adjustable Nozzle of the Ames 6- by 6-Foot Supersonic Wind Tunnel. NACA RM A9E24, 1949.
- 6. Glauert, H.: Wind Tunnel Interference on Wings, Bodies and Airscrews. R. & M. No. 1566, British A.R.C., 1933.

- 7. Herriot, John G.: Blockage Corrections for Three-Dimensional-Flow Closed-Throat Wind Tunnels, With Consideration of the Effect of Compressibility. NACA Rep. 995, 1950. (Formerly NACA RM A7B28)
- 8. Lessing, Henry C.: Aerodynamic Study of a Wing-Fuselage Combination Employing a Wing Swept Back 63° Effect of Sideslip on Aerodynamic Characteristics at a Mach Number of 1.4 With the Wing Twisted and Cambered. NACA RM A50F09, 1950.
- 9. Perkins, Edward W.: Experimental Investigation of the Effects of Support Interference on the Drag of Bodies of Revolution at a Mach Number of 1.5. NACA TN 2292, 1951.
- 10. Hall, Charles F., and Heitmeyer, John C.: Aerodynamic Study of a Wing-Fuselage Combination Employing a Wing Swept Back 63°. Characteristics at Supersonic Speeds of a Model With the Wing Twisted and Cambered for Uniform Load. NACA RM A9J24, 1950.

TABLE I .- AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 AND AN ALL-MOVABLE HORIZONTAL TAIL; R=3.8 × 106 (a) Characteristics for wing-body combination with horizontal tail removed (vertical fins not removed)

М	α	CL	CD	Cm	М	α	CL	CD	Cm	М	α	CL	$c_D$	Cm
0.60	-4.28	-0.260	0.0251	0.004	0.90	-4.38	-0.307	0.0290	0.016	1.50	8.32	0.415	0.0712	-0.062
	-2.14	133	.0126	.004		-2.18	154	.0130	.010	1	10.39	.510	.1024	077
	52	044	.0089	.003		53	047	-0084	.005		12.47	.601	.1401	092
1	.52	.014	.0084	.002		.50	.022	.0080	.001					
	2.11	.104	.0111	.001		2.16	.130	.0117	005	1.70	-4.14	197	.0280	.029
	4.25	.231	.0218	0		4.35	.285	.0265	012		-2.07	103	.0176	:016
	6.39	•355	.0416	.002		6.55	.434	.0528	015		50	029	.0139	.005
2.0	8.53	.474	.0710	.010		8.73	.564	.0884	016		.48	.017	.0137	002
	10.66	.582	.1096	.016		10.85	.660	.1294	017		2.06	.090	.0170	012
	12.77	.662	.1475	.030							4.14	.185	.0271	026
	14.86	.741	.1940	.033	1.30	-4.18	258	.0322	.040		6.21	.274	.0427	039
	16.97	.827	.2487	.034		-2.09	132	.0193	.021		8.28	.363	.0648	053
	18.02	.870	.2789	.034		50	062	.0242	.012		10.34	.447	.0926	067
- 0-	1 41	-01				.49	.021	.0145	002		12.41	.529	.1260	079
0.80	-4.34	286	.0275	.009	100	2.08	.115	.0185	016		14.46	.580	.1581	087
277	-2.17	146	.0130	.007		4.17	.240	.0307	036		1	100	20.51	000
	53	045	.0087	*004		6.26	.364	.0511	054	1.90	-4.13	175	.0264	.023
	.53	.019	.0084	002		8.35	.480	.0797	073		49	091	.0145	.012
	2.14	.117	.0114	001		10.43	.588	.1161	087	1 3 3	.48	.013	.0142	002
	6.49	.396	.0475	005	1.50	-4.16	225	.0297	.034		2.05	.078	.0167	011
	8.65	.514	.0788	.005	1.50	-2.08	116	.0179	.018		4.11	.161	.0251	023
1	10.78	.609		.007		50		.0138	.006		6.18	.240	.0389	034
	12.91	.707	.1155	.006		50	033	.0137	001		8.24	.319	.0584	046
	15.03	.799	.2140	.002	1000	2.07	.102	.0173	014		10.30	.395	.0831	058
	17.03	. 199	.2140	-002		4.16	:210	.0283	014	1	12.36	.469	.1129	068
		1		118		6.24	.314	.0462	045		14.42	.540	.1475	078
			1000	100			- 324	1000			15.97	.593	.1771	084

(b) Characteristics for wing-body-tail combination;  $\delta_n = +4^{\circ}$ 

М	α	CL	C <sub>D</sub>	Cm	Ch	8	М	Œ.	CL	CD.	Cm	ch	8	М	α	CL	CD	Cm	c <sub>h</sub>	8
0.60	-4.31	-0.225	0.0256	-0.026	0.015	4.0	0.90	-4.41	-0.257	0.0306	-0.028	0.014	4.0	1.50	4.12	0.264	0.0362	-0:085	-0.040	3.9
0.00	-2.15	087	.0140	033	.017	4.0	,.	-2.21	100	.0169	042	.007	4.0		6.20	.379	.0574	111	049	3.9
	48	.014	.0117	040	.018	4.0		49	.023	.0132	054	.004	4.0		7.81	.458	.0783	130	055	3.9
	.53	.077	.0126	045	.018	4.0		.54	.096	.0145	062	.003	4.0				Part of the same			
	2.14	.178	.0178	053	.018	4.0.		2.19	.214	.0214	074	0	4.0	1.70	-4.15	188	.0290	.020	004	4.0
	4.29	.314	.0327	060	.015	4.0		4.38	.375	.0406	086	0	4.0		-2.08	087	.0192	001	011	4.0
	6.44	.448	.0576	063	.010	4.0		6.58	•532	.0717	095	001	4.0		54	007	.0161	019	017	4.0
	8.59	.572	.0911	059	.003	4.0		8.77	.677	.1142	105	006	4.0		.48	*044	.0163	030	022	4.0
	10.72	.689	.1326	058	.002	4.0		10.91	.794	.1642	120	027	4.0	- 1	2.04	.125	.0210	047	028	3.9
	12.83	.774	.1763	047	.001	4.0		12.39	.887	.2071	143	044	3.9		4.11	.229	.0334	071	038	3.9
	14.94	.869	.2314	054	006	4.0									6.18	.329	.0521	093	048	3.9
	17.05	.968	•2957	061	015	4.0	1.30	-4.19	243	.0343	.024	006	4.0	177	8.25	.426	.0776	116	056	3.9
	18.11	1.019	.3312	064	021	4.0		-2.10	106	.0218	006	014	4.0			- (-			000	1. 0
						0.8		56	010	.0180	028	021	4.0	1.90	-4.13	167	.0275	.015	002	4.0
0.80	-4.37	239	.0268	028	.021	4.0		.48	.059	.0184	044	024	4.0		-2.07	076	.0191	003	009	4.0
	-2.19	093	.0147	038	.023	4.0		2.04	.159	.0239	067	032	3,9	12.00	54	008	.0168	017	015	4.0
	48	.020	.0122	048	.024	4.0		4.13	.299	.0395	101	041	3.9		.47	.037	.0172	026	019	4.0
	•54	.089	.0132	054	.024	4.0		6.21	.424	.0626	131	050	3.9	1000	2.03	.106	.0207	040	027	3.9
	2.17	.198	.0191	063	.024	4.0			010		001	ook	1.0		4.10	.198	.0312	058	046	3.9
	4.35	.344	.0358	071	.022	4.0	1.50	-4.17	213	.0312	.024	004	4.0		8.21		.0696		055	3.9
	6.53	.489	.0638	076	.015	4.0		-2.09	096	.0197	002	013	4.0			.370	.0090	096	063	3.9
	8.70	.611	.0995	070	.007	4.0		55	008	.0162	+.022	019	4.0		10.27	•471	.0912	114	005	3.9
	10.83	.714	.1413	075	.004	4.0	1	.48	.052	.0166	036	024	3.9							
	12.96	.823	.1942	083	004	4.0	1	2.05	.143	.0218	050	031	3.9							_

TABLE I .- AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 AND AN ALL-MOVABLE HORIZONTAL TAIL; R=3.8  $\times$  10<sup>6</sup> - Continued (c) Characteristics for wing-body-tail combination;  $\delta_{\rm n}$  = +2<sup>o</sup>

М	α	CL	CD	Cm	Ch	8	М	α	C <sub>L</sub>	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	δ
0.60	-4.27	-0.240	0.0245	-0.009	0.008	2.1	0.90	-4.37	-0.279	0.0289	-0.003	0.017	2.1	1.50	4.13	0.252	0.0335	-0.072	029	2.0
	-2.16	108	.0130	015	.010	2.1		-2.21	123	.0141	016	.016	2.1	1	6.21	.367	.0542	099	038	2.0
	53	011	.0099	022	.010	2.1		55	007	.0103	028	.014	2.1		8.28	.477	.0824	126	046	2.0
	.51	.052	.0103	027	.011	2.1		.53	.067	.0110	037	.013	2.1	1						
	2.13	.153	.0148	034	.013	2.1		2.18	.187	.0171	050	.010	2.1	1.70	-4.14	195	.0283	.029	.005	2.1
	4.28	.291	.0286	042	.014	2.1		4.38	.350	.0352	065	.009	2.1		-2.07	092	.0181	.007	002	2.1
	6.43	.426	.0524	046	.016	2.1		6.59	.516	.0668	074	.005	2.1		54	015	.0147	009	008	2.1
	8.58	.554	.0861	043	.016	2.1		8.76	.651	.1068	086	002	2.1		.48	.035	.0148	020	012	2.1
	10.71	.669	.1268	042	.014	2.1									2.05	.116	.0192	038	018	2.1
	12.81	.747	.1702	031	.013	2.1	1.30	-4.19	-,258	.0337	.038	.004	2.1	1	4.12	.218	.0310	060	027	2.0
	14.92	.847	.2255	040	.008	2.1		-2.09	119	.0208	.008	003	2.1		6.18	.317	.0490	083	036	2.0
	17.04	.958	.2923	052	002	2.1		55	019	.0167	014	010	2.1		8.25	-414	.0737	105	044	2.0
	18.09	.999	.3247	056	008	2.1		.48	.047	.0166	029	014	2.1		10.11	.497	.1012	125	052	2.0
		3			1			2.06	.151	.0220	052	020	2.1		1 20				200	
0.80	-4.33	259	.0267	007	.011	2.1		4.14	.290	.0372	086	029	2.0	1.90	-4.18	171	.0272	.022	.007	2.1
	-2.19	115	.0134	016	.012	2.1		6.23	.427	.0609	116	037	2.0		-2.06	081	.0185	.004	0	2.1
	54	007	.0100	026	.015	2.1		7.18	.486	.0747	130	042	2.0		53	013	.0161	009	006	2.1
	.52	.062	.0103	033	.016	2.1		1.00	000	0000	0.01	001		1	2.04	.100	.0194		018	2.1
	2.16	.174	.0158	043	.019	2.1	1.50	-4.16	223	.0302	.034	.004	2.1		4.10	.190	.0294	032	027	2.0
	4.34	. 324	.0317	053	.021	2.1		-2.08	104	.0186	.008	003	2.1		6.16	.276	.0450	068	035	2.0
	6.52	.471	,0589	060	.021	2.1		54	018	.0146	011	009	2.1	1	8.21	.361	.0666	087	043	2.0
	8.69	-595	10946	056	.022	2.1			.041	.0148	024	013	2.1		10.27	.441	.0935	104	051	2.0
	10.81	.694	.1352	059	.022	2.1		2.05	.133	.0198	044	050	2.1		12.33	.521	.1265	122	059	2.0
	12.96	.814	.1897	074	.022	2.1	8			A. H.					15.33	· SET	ر معد،	755	079	2.0

(d) Characteristics for wing-body-tail combination;  $\delta_n = 0^{\circ}$ 

М	α	CL	CD	Cm	Ch	8	М	α	CL	$c_{\mathrm{D}}$	Cm	Ch	8	М	α	$c_{L}$	$c_{\mathrm{D}}$	Cm	ch	8
0.60	-4.27	-0.266	0.0258	0.010	0.004	0.1	0.90	-4.36	-0.311	0.0307	0.020	0.004	0.1	1.50	4.18	0.243	0.0319	-0.060	-0.023	0.1
	-2.11	131	.0133	.004	.004	.1		-2.16	150	.0144	.008	.006	.1	1.70	6.28	.359	.0525	087	032	0.1
	50	035	.0097	003	.002	.1		48	038	.0099	002	.007	.1		8.35	.470	.0806	114	041	.1
	.56	.030	.0095	008	.003	.1		.58	.040	.0098	011	.008	.1	1			,,,,,,,		-1041	**
	2.17	.129	.0131	016	.004	.1		2.22	.159	.0146	024	.008	.1	1.70	-4.13	207	.0292	.039	.011	.1
100	4.30	,264	.0254	023	.005	.1		4.40	.319	.0313	039	.010	.1		-2.07	101	.0182	.016	.002	.1
	6.48	.400	.0482	027	.008	.1	1773	6.63	.480	.0609	049	.011	.1		44	023	.0145	0	003	.1
	8.63	.525	.0802	023	.010	.1		8.81	.621	.1007	060	.008	.1		.56	.029	.0144	012	007	.1
	10 77	.645	.1228	023	.012	.1				S Trees to					2.11	.110	.0185	029	014	.1
	12.84	.718	.1615	011	.012	.1				1					4.17	.212	.0298	050	022	.1
	14.93	.822	.2160	021	.013	.1	1.30	-4.16	274	.0347	.054	.011	.1		6.26	.313	.0479	073	032	0
	17.02	.928	.2793	035	.011	.1		-2.06	132	.0206	.023	.002	.1		8.33	.411	.0725	095	040	0
	18,06	.978	.3136	043	.005	.1		45	031	.0160	.001	003	.1		10.40	.502	.1033	116	049	0
0.80	-4.32	287	0000	03.5		Mar are		.56	.035	.0161	014	008	.1							
0.00	-2.14	140	.0280	.015	.004	.1		2.12	.139	.0210	038	015	.1	1.90	-4.11	180	.0279	.029	.011	.1
	51	036	.0097	004	.003	.1		4.19	.277	.0354	070	023	.1		-2.04	088	.0186	.012	.002	.1
- 11	.57	.035	.0096	011	.003	.1		6.31	.416	.0590	102	032	0		44	020	.0160	001	002	.1
	2.20	.144	.0137	020	.005	.1	130	8.39	.542	.0909	132	041	0		-55	.026	.0159	011	007	.1
- 1	4.36	.290	.0280	031	.008	.1	1.50	-4.14	239	.0312	.047	033			2.10	.095	.0189	024	014	.1
	6.57	.441	.0544	038	.011	.1	1.0	-2.05	116	.0184		.011	0		4.15	.183	.0284	042	024	0
100	8.73	.562	.0880	033	.014	.1		45	028	.0142	.020	002	0		6.24	.270	.0440	059	031	0
	10.86	.659	.1271	036	.014	.1		.56	.032	.0143	012	002	.1		8.30	•355	.0654	078	041	0
+	12.98	.783	.1805	051	.018	.1		2.11	.124	.0188	033	015	.1		10.36	.435	.0920	095	049	0

TABLE I .- AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 AND AN ALL-MOVABLE HORIZONTAL TAIL; R=3.8  $\times$  10<sup>6</sup> - Continued (e) Characteristics for wing-body-tail combination;  $\delta_n$  = -2<sup>o</sup>

М	a	CL	$c_{\mathrm{D}}$	Cm	Ch	δ	М	α	CL	c <sub>D</sub>	Cm	ch	8	М	a.	CL	c <sub>D</sub>	Cm	C <sub>h</sub>	8
0.60	-4.29	-0.283	0.0273	0.026	0	-1.9	0.90	-4.39	-0.335	0.0327	0.042	0.003	-1.9	1.50	8.29	0.453	0.076	0.100		
	-2.14	150	.0139	.020	.001	-1.9	0.70	-2.19	172	.0152	.028	.002	-1.9		10.10	.545	0.0764	-0.100 122	-0.029	-2.0
	52	053	.0099	.013	.002	-1.9		54	058	.0099	.015	001	-1.9	- 14	10.10	• )4)	.1057	122	037	-2.0
	.52	.010	.0095	.008	.002	-1.9		.54	.019	.0096	.007	0	-1.9	1.70	-4.13	215	.0301	.047	.021	-1.9
	2.11	.106	.0126	.002	001	-1.9		2.16	.130	.0137	003	0	-1.9	1.10	-2.06	110	.0186	.025	.012	-1.9
	4.26	.243	.0243	007	001	-1.9		4.36	.292	.0293	016	.004	-1.9		49	031	.0145	.008	.005	-1.9
	6.41	-377	.0461	010	.002	-1.9		6.57	.452	.0575	025	.006	-1.9		.48	.018	.0142	003	.001	-1.9
	8.56	.504	.0773	006	.003	-1.9		8.75	-593	.0963	034	.008	-1.9		2.06	.098	.0179	019	003	-1.9
	10.69	.617	.1168	005	.005	-1.9								100	4.13	.200	.0287	041	011	-1.9
	12.79	.696	.1569	.007	.005	-1.9	1.30	-4.16	287	.0362	.070	.022	-1.9		6.20	.296	.0454	062	020	-1.9
	14.90	.796	.2096	002	.007	-1.9		-2.08	147	.0215	.038	.013	-1.9		8.26	.394	.0692	084	028	-2.0
	17.01	.900	.2710	016	.010	-1.9		50	043	.0162	.014	.006	-1.9		10.32	.485	.0987	105	038	-2.0
	18.08	.959	.3078	024	.011	-1.9		.49	.021	.0160	0	.002	-1.9						1.55	-
0.00	1 00					Smart		2.07	.122	.0200	~.022	002	-1.9	1.90	-4.12	188	.0287	.037	.023	-1.9
0.80	-4.35	309	.0297	.033	0	-1.9		4.16	.258	.0332	~.054	010	-1.9	12	-2.06	097	.0190	.019	.013	-1.9
	-2.17	162	.0144	.024	.001	-1.9		6.25	-395	.0554	~.085	018	-1.9		49	027	.0160	.005	.006	-1.9
	53	056	.0097	.015	,002	-1.9		8.33	.522	.0862	~.115	028	-2.0		.48	.015	.0159	003	.002	-1.9
	.53 2.14	.012	.0093	.009	0	-1.9			-10						2.05	.085	.0184	017	003	-1.9
		.267	.0127	001	0	-1.9	1.50	-4.24	248	.0330	.058	.022	-1.9	7.1	4.11	.173	.0276	034	013	-1.9
	6.49		.0263	011	0	-1.9		-2.07	128	.0193	.031	.012	-1.9	100	6.17	.259	.0423	051	021	-1.9
	8.66	.411	.0508	017	.002	-1.9		49	035	.0145	.011	.005	-1.9	1 1 2 2 3	8.23	.343	.0630	069	029	-2.0
118	10.79	.536 .634	.0841	013	.004	-1.9	1000	.49	.020	.0143	~,001	.001	-1.9	X 1	10.28	.423	.0890	086	037	-2.0
			.1220	013	.004	-1.9	11000	2.07	.110	.0182	021	003	-1.9		12.34	.502	.1205	102	045	-2.0
	12.93	.750 .818	.1736	025	.007	-1.9	127	4.14	.228	.0304	047	011	-1.9	NINA.	14.40	.579	.1578	118	052	-2.0
	14,00	.010	.2055	039	.011	-1.9		6.22	.342	.0496	~.074	019	-1.9							

(f) Characteristics for wing-body-tail combination;  $\delta_n = -4^{\circ}$ 

М	α	$c_{\rm L}$	CD	Cm	Ch	δ	М	α	$c_{L}$	CD	Cm	ch	8	М	α	CL	CD.	Cm	ch	δ
0.60	-4.29	-0.311	0.0303	0.045	-0.011	-3.9	0.90	0.55	-0.014	0.0100	0.034	-0.003	-3.9	1.70	-4.12	-0.227	0.0320	0.058	0.029	-3.
	-2.14	180	.0159	.039	009	-3.9		2.24	.108	.0135	.020	005	-3.9		-2.04	122	.0198	.035	.020	-3.
	49	079	.0107	.032	008	-3.9		4.38	.265	.0277	.005	003	-3.9		44	040	.0152	.018	.013	-3.
	.53	016	.0097	.027	007	-3.9		6.61	.424	.0553	004	002	-3.9		.60	.013	.0147	.006	.009	-3.
	2.18	.083	.0123	.019	005	-3.9		8.79	.570	.0939	014	002	-3.9		2.11	.090	.0179	010	.002	-3
	4.28	.218	.0227	.011	004	-3.9									4.17	.191	.0283	031	006	-3
	6.46	.354	.0440	.007	003	-3.9	1.30	-4.14	303	.0387	.086	.027	-3.8		6.27	.290	.0450	053	014	-3
	8.60	.476	.0737	.011	002	-3.9		-2.05	161	.0230	.054	.021	-3.9	100	8.34	.387	.0677	075	022	-3
	10.75	.593	.1129	.012	001	-3.9		45	057	.0171	.030	.014	-3.9		10.41	.479	.0975	095	031	-4
	12.82	.669	.1522	.025	0	-3.9	100	.61	.012	.0166	.015	.010	-3.9		12.44	.567	.1325	115	040	-14
								2.13	.111	.0202	~.008	.004	-3.9							1
.80	-4.35	339	.0331	.057	015	-3.9		4.21	.246	.0327	~.039	003	-3.9	1.90	-4.10	195	.0296	.045	.028	-3
	-2.16	196	.0166	.048	013	-3.9		6.33	.381	.0542	070	010	-3.9		-2.03	105	.0195	.027	.019	-3
	51	088	.0097	.038	011	-3.9		8.41	.509	.0844	~.100	018	-3.9		44	035	-0161	.013	.011	-3
	.54	015	.0096	.031	008	-3.9		10.19	.608	.1165	~.121	025	-4.0		.59	.012	.0159	.004	.006	-3
	2.22	.095	.0126	.020	006	-3.9									2.10	.077	.0182	009	0	-3
	4.34	.239	.0249	.010	003	-3.9	1.50	-4.13	261	.0347	.073	.029	-3.8		4.15	.165	.0268	026	008	-3
	6.56	.391	.0496	.003	002	-3.9	1	-2.04	139	.0205	.044	.021	-3.9		6.24	.250	.0413	043	017	-3
	8.72	.509	.0811	.008	0	-3.9		44	047	.0152	.023	.014	-3.9		8.30	-334	.0614	060	025	-4
	10.85	.607	.1185	.008	0	-3.9		.61	.014	.0149	.010	.010	-3.9		10.36	.414	.0871	077	033	-4
	1. 00	200	0000	0770	000			2.13	.102	.0185	~.010	•005	-3.9		12.39	.491	.1179	093	040	-4
.90	-4.38	372	.0376	.073	.007	-3.9		4.19	.218	.0226	~.036	004	-3.9		14.43	.565	.1536	108	047	-4
	-2.18	209	.0182	.057	.001	-3.9		6.30	•334	.0494	~.062	012	-3.9		15.46	.604	.1743	115	052	-4
	51	091	.0112	*011	002	-3.9		8.37	.442	.0753	~.088	020	-3.9					1 1		
	-	7					1	10.45	.547	.1086	~.113	-,029	-4.0					0.00		

TABLE I.- AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 AND AN ALL-MOVABLE HORIZONTAL TAIL;  $R=3.8 \times 10^6$  - Continued

(g) Characteristics for wing-body-tail combination;  $\delta_n = -8^{\circ}$ 

М	α	CL	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	8
0.60	-4.32	-0.348	0.0387	0.074	0.008	-8.0	0.90	-4-40	-0.404	0.0467	0.105	0.012	-8.0	1.50	6.24	0.306	0.0475	-0.039	0.005	
	-2.18	222	.0228	.071	.002	-8.0		-2.21	253	.0268	.097	.012			8.32	.418	.0726	064	001	
	57	127	.0163	.066	003	-8.0		57	138	.0188	.086	.009			10.39	.520	.1043	088	009	
	.42	067	.0141	.062	007	-8.0		.43	072	.0164	.080	.008	-8.0		11.74	.587	.1292	103	015	-8.
	2.10	.032	.0140	.056	011			2.17	.048	.0168	.068	.003	-8.0							
	4.27	.171	.0225	.046	013			4.38	.214	.0287	.053	001	-8.0	1.70	-4.12	244	.0368	.077	.047	
	6.42	.307	.0409	.042	011			6.58	.370	.0525	-044	0	-8:.0		-2.05	138	.0233	.053	.038	
	8.56	.435	.0692	.044	010			8.72	.508	.0864	.037	.003		1	49	058	.0180	.035	.030	
	10.65	.548	.1027	.045	008			10.85	.608	.1266	.031	.020	-8.0		49	007	.0171	.025	.025	
	12.80	.628	.1420	.059	008										2.12	.073	.0196	.008	.018	
	14.86	.722	.1908	.050	005		1.30	-4.14	329	.0454	.110		-7.9		4.15	.171	.0285	013	.009	
	16.98	.826	.2489	.037	003	-8.0		-2.05	190	.0283	.081		-7.9		6.21	.267	.0438	033	.001	
	18.04	.882	.2823	.029	002	-8.0		49	088	.0515	.057		-7.9	1	8.28	.363	.0659	052	005	
								.49	023	.0196	.044		-7.9		10.35	.454	.0941	073	014	
.80	-4.38	385	.0430	.092	016	-8.0		2.14	.083	.0555	.020	.022		1	12.41	.542	.1286	093	023	-8.
	-2.20	241	.0241	.084	018			4.19	.215	.0327	010	.017								
	58	135	.0168	.076	019			6.27	.349	.0521	040	.009		1.90	-4.11	212	.0336	.060	.044	
	.43	071	.0145	.071	020	-8.0		8.36	-479	.0810	069	.002			-2.04	119	.0223	.041	.034	
	2.13	.039	.0148	.062	020			10.44	-594	.1176	093	004	-8.0		49	050	.0185	.028	.027	
	4.33	.189	.0246	.051	019				-01	-1		-10	-	l l	.48	005	.0177	.019	.055	
	6.51 8.67	·337	.0458	.043	017	-8.0	1.50	-4.13	286	.0412	.097		-7.9		2.10	.063	.0196	.006	.014	
1 4	10.80		.0754	.048	015			-2.05	162	.0251	.067		-7.9		4.12	.150	.0274	011	.005	
	12.89	.556	.1099	.050	014			49	070	.0186	.045		-7.9		6.18	.232	.0408	026	002	
	15.02	.782	.1543	.038	009			.49	012	.0175	.033		-7.9		8.24	.316	.0603	042	010	
	17.02	. 105	.2110	.015	003	-8.0		2.13	.079	.0202	.012	.022	-8.0		10.30	.396	.0853	058	019	-B.
				3			1	4.17	.195	.0302	014	.013	-8.0		12.36	.473	.1154	074	026	

(h) Characteristics for wing-body-tail combination;  $\delta_{\rm n} = -12^{\circ}$ 

М	α	$c_{\mathrm{L}}$	c <sub>D</sub>	Cm	ch	8	М	α	CL	CD	Cm	Ch	8	М	α	$c_{L}$	$c_{\mathbb{D}}$	Cm	Ch	8
0.60	-4.31	-0.348	0.0454	0.077	0.030	-12.0	0.90	2.16	0.037	0.0238	0.079	0.027	-12.0	1.70	-4.11	-0.267	0.0448	0.098	0.062	-11.
0.00	-2.17	224	.0299	.078		-12.0	0.,0	4.38	.183	.0358	.081	.017			-2.04	158	.0296	.073	.055	
	57	134	.0236	.077		-12.0		6.58	-339	.0587	.074		-12.0		49	080	.0235	.054		-11.
	.41	081	.0214	.076		-12.0		8.76	.475	-0919	.071		-12.0		.49	027	.0220	.043	.044	-11.
	2.08	.011	.0208	.074		-12.0		10.89	.568	.1318	.075		-11.9		2.12	.054	.0239	.027		-11.
	4.25	.140	.0277	.071		-12.0			.,,,,	7.55	12		,		4.16	.154	.0319	.006	.025	
	6.40	.272	.0445	.070		-12.0	1.30	-4.14	354	.0542	.133	.069	-11.9		6.23	.251	.0462	014	.015	
	8.55	-395	.0703	.075		-12.0	1.50	-2.04	214	.0364	.105		-11.9		8.29	.345	.0670	033	.006	-12.
	10.68	.507	.1028	.078		-12.0		47	113	.0287	.084		-11.9		10.36	.436	.0939	053	0	-12.
	12.78	.587	.1377	.093		-12.0		.50	049	.0266	.070		-11.9		12.42	.525	.1276	072	009	-12.
	14.88	.674	.1817	.087		-12.0		2.15	.056	.0281	.047		-11.9		13.82	.580	.1529	084	014	-12
	21100		12021		100			4.24	.191	.0381	.017		-11.9		-		-			100
08.0	-4.36	355	.0459	.074	.030	-12.0		6.29	.322	.0553	011		-11.9	1.90	-4.10	227	.0398	.077	.059	-11.
,,,,,	-2.19	221	.0292	.074		-12.0		8.38	.452	.0827	039		-12.0		-2.04	136	.0277	.057	.049	-11.
	57	124	.0229	.073		-12.0		10.46	.567	.1180	064		-12.0		49	066	.0231	.043		-11
	.43	066	.0210	.073		-12.0	1	11.34	.611	.1352	072		-12.0	1	.48	023	.0220	.035	.036	-11
	2.14	.034	.0212	.070		-12.0									2.10	.048	.0234	.022	.029	
	4.33	.172	.0306	.067		-12.0	1.50	-4.12	308	.0494	.116	.056	-11.9		4.13	.134	.0307	.005	.020	-12.
	6.51	-313	.0510	.066		-12.0		-2.04	193	.0335	.094		-11.9		6.19	.217	.0434	010	.010	-12
	8.67	.434	.0791	.073	.002	-12.0		48	097	.0257	.071	.048	-11.9		8.25	.298	.0618	026	.001	-12
	10.80	.528	.1123	.076		-12.0		.49	038	.0236	.056		-11.9		10.31	.379	.0861	040	005	-12
	12.93	.628	.1561	.075	008	-12.0		2.14	.056	.0252	.036	.040	-11.9		12.36	.456	.1153	055	015	-12
			1	1	1		1	4.18	.172	.0339	.009	.031	-11.9	1	14.42	.531	.1500	069	021	-12
0.90	-4.40	385	.0498	.088	.035	-11.9		6.25	.284	.0497	016	.021			16.18	.595	.1841	080	026	-12
	-2.20	232	.0306	-080		-11.9		8.33	. 394	.0732	040	.012	-12.0							
	56	124	.0234	.077		-11.9		10.40	.498	.1040	064	.006	-12.0							
	.44	063	.0213	.074		-11.9		12.47	-597	.1420	086	0	-12.0	1						

TABLE I. - AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 AND AN ALL-MOVABLE HORIZONTAL TAIL; R=3.8 × 10<sup>6</sup> - Continued

(i) Characteristics for wing-body-tail combination;  $\delta_n = -16^\circ$ 

М	α	CL	C <sub>D</sub>	Cm	Ch	8	М	α	$c_{L}$	c <sub>D</sub>	Cm	Ch	8	М	α	CL	C <sub>D</sub>	Cm	Ch	8
0.60	-4.31	-0.332	0.0481	0.068	0.031	-16.0	0.90	-2.20	-0.231	0.0358	0.082	0.038	-16.0	1.50	10.41	0.473	0.1067	-0.041	0.018	-16.
0.00	-2.16	208	.0331	.068	.030	-16.0		56	122	.0291	.077	.037	-16.0		12.48	-573	.1434	064	.010	-16.
	56	118	.0279	.068	.030	-16.0		.45	058	.0270	.074	.037	-16.0							
1.00	.43	064	.0262	.067	.031	-16.0		2.18	.053	.0287	.068	.036	-16.0	1.70	-4.10	285	.0546	.117	.062	-15
	2.10	.024	.0268	.068	.031	-16.0		4.38	.207	.0405	.061	.035	-16.0		-2.02	180	.0390	.095	.061	-15
4,50	4.26	.142	.0345	.073	.032	-16.0		6.59	.359	.0648	.058	.035	-16.0		47	098	.0314	.075	.057	-15.
	6.40	.265	.0512	.077	.029	-16.0		8.77	.495	.0996	.058	.034	-16.0		.49		.0292	.063	.054	-15
1113	8.55	.386	.0778	.086	.021	-16.0					-1-	000	350		4.21	.033	.0300	.046	.048	-15 -15
	10.68	.493	.1092	.093	.016	-16.0	1.30	-3.09	307	.0552	.142	.080	-15.8		6.23	.135	.0504	.004	.027	-15
	12.78	.567	.1428	.109	.015	-16.0		-2.03	236	.0468	.128	.077	-15.8 -15.9		8.30	.323	.0704	015	.018	-16
	14.87	.644	.1839	.109	.010	-16.0 -16.0	100	46	137	.0381	.094	.066	-15.9		10.37	.413	.0964	034	.010	-16
	16.97	.735	.2350	.104	003	-16.0		2.15	.030	.0359	.070	.058	-15.9		12.43	.501	.1284	053	.003	-16
	18.02	.779	.2624	.098	003	-10.0		4.26	.167	.0446	.040	.046	-15.9		14.50	.583	.1665	069	003	-16
.80	1, 26	355	.0508	.076	.032	-16.0		6.30	.295	.0612	.013	.037	-15.9	7 7324		.,				
.00	-4.36 -2.18	216	.0338	.073	.031	-16.0		8.39	.423	.0872	013	.031	-15.9	1.90	-4.09	246	.0478	.095	.073	-15
	56	118	.0277	.070	.031	-16.0		10.47	.535	.1210	035	.029	-15.9		-2.03	152	.0345	.074	.063	-15
	44	058	.0259	.068	.030	-16.0		11.91	.610	.1488	050	.023	-16.0		48	082	.0291	.059	.054	-15
	2.14	.042	.0266	.064	.031	-16.0						197			.48	038	.0276	.051	.049	-15
	4.33	.179	.0364	.062	.031	-16.0	1.50	-4.11	325	.0594	.133	.068	-15.9		2.10	.030	.0283	.038	.041	-15
	6.51	.320	.0577	.065	.031	-16.0		-2.03	206	.0423	.109	.062	-15.9		4.18	.119	.0349	.021	.031	-15
	8.67	.434	.0861	.074	.029	-16.0		47	116	.0344	.090	.057	-15.9		6.20	.200	.0470	.006	.021	-16
	10.80	.531	.1201	.079	.026	-16.0		.49	062	.0323	.078	.054	-15.9		8.26	.281	.0648	010	.013	-16
	12.92	.612	.1601	.085	.022	-16.0	189	2.14	.030	.0329	.059	.049	-15.9		10.31	.361	.0881	024	005	-16 -16
	15.03	.700	.2089	.082	.001	-16.0		4.23	.149	.0406	.032	.043	-15.9		12.37	.437	.1167	051	010	-16
		-0-		001	000	360	3 2 10	6.27	.261	.0551	018	.036	-15.9 -15.9		16.49	.586	.1899	064	016	-16
.90	-4.40	385	.0551	.091	.038	-16.0		. 8.34	•370	.0774	010	.020	-17.9	1	10.49	.,00	12099	004	.010	1

(j) Characteristics for wing-body-tail combination;  $\delta_n = -20^{\circ}$ 

M	α	C <sub>L</sub>	c <sub>D</sub>	Cm	ch	8	м	α	C <sub>L</sub>	$c_{\mathrm{D}}$	Cm	$c_{\rm h}$	8	м	α	CL	$c_{\mathrm{D}}$	Cm	Ch	δ
0.60	4.30	-0.331	0.0541	0.071	0.032	-19.9	0.90	4.38	-0.387	0.0623	0.098	0.046	-19.8	1.50	10.42	0.449	0.1104	-0.019	0.043	-19.
.00	-2.16	208	.0394	.071	.030	-19.9	0.,0	-2.19	236	.0430	.089	.044	-19.8		12.49	.547	.1453	042	.033	-19
	56	118	.0335	.069	.030	-19.9		56	128	.0361	.084	.045	-19.8							
	.43	062	.0317	.069	.029	-19.9		.45	063	.0340	.080	.045	-19.8	1.70	4.09	297	.0650	.130	.077	-19
	2.09	.024	.0315	.066	.029	-19.9		2.16	.045	.0345	.073	.042	-19.8	The state of the s	-2.01	196	.0500	.111	.072	-19
	4.26	.153	.0393	.066	.030	-19.9		4.37	.201	.0468	.066	.040	-19.8		46	119	.0425	.096	.070	-19
	6.40	.276	.0564	.068	.032	-19.9		6.57	.354	.0711	.061	.039	-19.8	100	.49	070	.0398	.085	.069	-19
	8.54	396	.0831	.077	.034	-19.9		8.75	.492	.1055	.058	.041	-19.8	1	2.12	.012	.0392	.066	.066	-19
	10.67	.496	.1148	.088	.035	-19.9	- 1	10.89	.586	.1467	.070	.050	-19.8	- 1000	4.22	.116	.0447	.044	.059	-19
	12.77	.568	.1490	.108	.035	-19.9			.,			1	100		6.28	.212	.0569	.022	.049	-19
	14.85	.632	.1907	.116	.032	-19.9	1.30	-2.02	251	.0582	.144	.096	-19.7		8.31	.305	.0753	.003	.040	-19
	16.95	.711	.2375	.118	.024	-19.9	2.50	49	155	.0490	.126	.091	-19.7	2505	10.37	.396	.1005	016	.031	-19
	18.00	.756	.2659	.116	.019	-19.9		.51	095	.0467	.115	.088	-19.7		12.44	.483	.1317	034	.021	-19
	20.00	.150			,	-,-,		2.15	.006	.0457	.093	.081	-19.7	L. Burgon	14.50	.566	.1686	051	.013	-19
.80	4.36	361	.0577	.082	.037	-19.8		4.26	.143	.0527	.062	.072	-19.8				100	700		1
	-2.18	221	.0405	.078	.036	-19.8		6.35	.273	.0685	.034	.063	-19.8	1.90	4.08	265	.0607	115	.066	-19
	56	123	.0339	.075	.034	-19.8		8.39	.396	.0929	.009	.056	-19.8	3,130	-2.02	171	.0457	.094	.071	-19
	.44	062	.0320	.072	.034	-19.8		10.47	.508	.1258	012	.051	-19.8	1 700	47	100	.0390	.079	.067	-19
	2.14	.039	.0325	.068	.034	-19.8		12.55	.612	.1658	030	.044	-19.8		.48	057	.0369	.070	.061	-19
	4.33	.179	.0421	.064	.034	-19.8							100		2.11	.013	-0365	.055	.052	-19
	6.50	.319	.0628	.063	.034	-19.8	1.50	-2.09	221	.0530	.126.	.082	-19.7		4.19	.103	.0422	.037	.040	-19
	8.66	.438	.0914	.072	.034	-19.8	1	. 46	134	.0444	.109	.078	-19.7	19900	6.25	.184	.0535	.021	.031	-19
	10.80	.538	.1265	.076	.034	-19.8		.49	081	.0418	.097	.074	-19.7	F ( )	8.27	.265	.0706	.006	.023	-19
	12.91	.619	.1675	.082	.034	-19.8		2.14	.010	.0415	.078	.067	-19.8		10.33	.345	.0935	009	.015	-19
	15.02	.706	.2167	.080	-033	-19.9		4.24	.127	.0485	-053	.059	-19.8		12.39	.421	.1212	022	.007	-19
	17.11	.770	.2655	.083	.023	-19.9		6.32	.237	.0621	.029	.055	-19.8		14.45	.494	.1540	035	.004	-19
	18.17	.810	.2958	.082	.008	-19.9		8.35	.345	.0826	.004	.052	-19.8		16.51	.568	.1924	048	0.	-1

TABLE I.- AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 AND AN ALL-MOVABLE HORIZONTAL TAIL;

 $R=3.8 \times 10^6$  - Concluded

(k) Characteristics for wing-body-tail combination;  $\delta_n = -24^\circ$ 

	CL.	CD	Cm	Ch	8	М	α.	$c_{L}$	CD	Cm	Ch	8	M	α	$c_{L}$	CD	Cm	Ch	δ
10	-0.336	0.0607	0.074	0.038	-23.9	0.90	-4.39	-0.393	0.0706	0.104	0.057	-23.8	1.50	10.44	0.428	0.1202	0.002	0.043	-23.
6	206	.0449	.073	.038	-23.9		-2.19	240	.0507	.096	.055	-23.8		12.52	.527	.1544	019	.038	-23.
6	119	.0393	.072	.038	-23.9		56	134	.0438	.090	.054	-23.8							
13	065	.0374	.070	.037	-23.9	1931	.45	070	.0417	.087	.052	-23.8	1.70	-4.09	305	.0758	.138	.080	-23
0	.025	.0377	.069	.036	-23.9		2.16	.040	.0422	.080	.048	-23.8		-2.01	209	.0615	.122	.075	-23
6	.152	.0451	.067	.036	-23.9		4.38	.199	.0545	.073	.046	-23.8		45	134	.0540	.108	.072	-23
1	.278	.0627	.069	.037	-23.9		6.58	.354	.0790	.067	.048	-23.8		.50	087	.0514	.099	.070	-23
56	.405	.0904	.077	.036	-23.9		8.76	.495	.1136	.061	.049	-23.8		2.12	008	.0509	.083	.065	-23
9	.507	.1224	.084	.035	-23.9									4.23	.093	.0562	.063	.062	-23
19	.581	.1578	.101	.038	-23.9	1.30	-2.02	265	.0719	.154	.101	-23.7		6.30	.192	.0670	.042	.060	-23
88	.657	.2018	.109	.040	-23.9		45	170	.0628	.138	.097	-23.7		8.32	.286	.0840	.020	.047	-23
97	.723	.2485	.114	.040	-23.9		.51	112	.0597	.127	.094	-23.7		10.39	.378	.1084	0	.034	-23
22	.758	.2752	.117	.038	-23.9		2.14	013	.0585	.107	.089	-23.7		12.46	.466	.1387	018	.023	-23
			0.1	The state of			4.26	.124	.0654	.078	.083	-23.7	1	14.52	.548	.1752	034	.016	-23
36	363	.0656	.086	.046	-23.8		6.34	.250	.0802	.052	.073	-23.8							
18	225	.0478	.083	.046	-23.8		8.38	.372	.1037	.029	.063	-23.8	1.90	-4.08	277	.0716	.124	.071	-2
56	127	.0417	.080	.045	-23.8	1	10.46	.483	.1352	.009	.056	-23.8		-2.01	190	.0586	.110	.067	-23
+4.	068	.0393	.077	.044	-23.8	1	12.54	.585	.1737	009	.050	-23.8		46	122	.0526	.098	.066	-23
14	.034	.0399	.073	.042	-23.8	100								.49	081	.0501	.091	.069	-2
33	.176	.0492	.069	.040	-23.8	1.50	-2.01	234	.0653	.136	.083	-23.7		2,11	006	.0477	.073	.068	-23
51	.315	.0697	.067	.039	-23.8		45	149	.0570	.121	.079	-23.7		4.20	.087	.0518	.053	.057	-23
58	.442	.0998		.038	-23.8		.51	098	.0544	.111	.076	-23.7		6.26	.172	.0626	.036	.047	-2
33	.547	.1362		.037	-23.8	128	2.14	009	.0539	.094	.070	-23.7		8.28	.251	.0786	.020	.038	-2
93	.628	.1770	.078	.037	-23.8		4.25	.109	.0637	.067	.064	-23.8		10.34	.331	.1009	.005	.026	-2
05	.718	.2272	.074	.040	-23.8		6.33	.221	.0726	.045	.056	-23.8		12.40	.408	.1282	009	.017	-2
15	.788	.2795	.075	.043	-23.8		8,37	.324	.0925	.024	.046	-23.8		14,46	.482	.1605	021	.009	-2
	13 4 13			1000		1	1000						1	16.52	.556	.1987	033	.004	-2

NACA

TABLE II. - AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 WITH LEADING-EDGE CHORD EXTENSIONS AND AN ALL-MOVABLE HORIZONTAL TAIL

(a) Characteristics for wing-body combination with horizontal tail removed (vertical fins not removed)

М	α	CL	CD	· Cm	М	α	O <sub>L</sub>	CD	Cm	М	α	CL	CD	Cm
0.60	4.30	-0.270	0.0264	0	0.90	0.51	0.024	0.0088	0.002	1.50	-0.52	-0.039	0.0151	0.00
	-2.16	144	.0138	.002		1.07	.061	.0092	0		.50	.019	.0146	00
	-1.07	079	.0103	.002		2.18	.135	.0118	002		1.03	.048	.0152	00
	52	046	.0095	.002		4.37	.288	.0253	007		2.08	.105	.0181	01
	.52	.017	.0091	.002		6.58	.448	.0526	013		4.17	.213	.0293	03
	1.04	.046	.0094	.002	100	8.77	.602	.0934	025		6.25	.320	.0475	04
	2.12	.107	.0111	.002		10.95	.763	.1470	050		8.33	.422	.0725	06
	4.25	.230	.0197	.002			11-0				10.40	.518	.1040	07
	6.40	•359	.0411	.005	1.20	4.22	308	.0356	.046				3.55	77
	8.54	.482	.0705	.009		-2.11	158	.0200	.025	1.70	4.16	206	.0303	.03
	10.68	.608	.1098	.009		-1.06	083	.0158	.014		-2.08	109	.0194	.01
	12.81	.729	.1578	.008		52	048	.0145	.009		-1.04	059	.0162	.01
	14.94	.834	.2128	.010		.50	.026	.0139	002		51	034	.0153	.00
	16.97	.910	.2671	.024		2.10	.132	.0178	017		.49	.018	.0148	00
	18.06	.917	.2897	.034		4.20	.276	.0311	039		1.03	.043	.0151	00
			1			1.04	.061	.0144	006		2.07	.093	.0175	01
0.80	4.37	297	.0293	.005		6.30	.420	.0543	061		4.15	.186	.0275	02
.00	-2.19	158	.0144	.005		8.41	.563	.0874	083		6.22	.281	.0438	04
	-1.10	083	.0104	.003			.,-5				8.29	.370	.0660	05
	54	048	.0092	.003	1.30	4.21	276	.0356	.041		10.36	.457	.0942	06
	.54	.020	.0086	.002		-2.10	143	.0212	.022		12.43	•539	.1277	07
	1.06	.052	.0091	.001	1500	-1.05	076	.0172	.012		12.43	•539	*T511	01
	2.15	.120	.0110	0		52	043	.0160	.007	1.90	4.14	180	.0286	.02
	4.32	.258	.0222	.001		.50	.023	.0155	002	1.90	-2.07	094	.0192	.01
	6.50	.394	.0454	.001		1.04	.055	.0160	007		-1.03	050	.0192	.00
	8.67	•535	.0801	.003		2.09	.119	.0192	016		50	028	.0160	.00
	10.84	.669	.1248	.011		4.18	.246	.0316	035		50	.016	.0156	00
	12.99	.793	.1778	.016		6.28	.372	.0523	054		1.02	.018	.0150	00
	12.99	•173	*1110	.010	1	8.37	.492	.0813	072		2.06	.030	-0180	01
0.90	-4.41	321	.0321	.011		10.46	.603	.1181	089		4.12	.164	.0265	01
0.30	-2.21	167	.0152	.007	1	10.40	.005	*****	,		6.19		.0407	03
	-1.11	090	.0105	.005	1.50	4.18	238	.0326	.036		8.25	.248	.0607	03
	55	050	.0094	.003	1.50	-2.09	126	.0201	.020		10.31	.327	.0853	05
	.,,	,0	,4		1	-1.05	068	.0163	.011			.404		06
	100				1	-1.0)	-,000	.0103	.JII		12.37		.1155	
100					H						14.43	-551	.1507	

TABLE II. - AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 WITH LEADING-EDGE CHORD EXTENSIONS AND AN ALL-MOVABLE HORIZONTAL TAIL - Continued

(b) Characteristics for wing-body-tail combination;  $\delta_n = +4^{\circ}$ 

М	α	CL	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	8
0.60	4.32	-0.229	0.0253	-0.027	0.016	4.0	0.90	0.56	0.092	0.0139	-0.054	0.020	4.1	1.50	1.02	0.084	0.0187	-0.043	-0.023	3.9
0.00	-2.16		.0139	032	.017	4.0		1.10	.131	.0153	057	.019	4.0		2.06	.147	.0230	057	028	3.9
	-1.06	019	.0114	036	.017	4.0		2.20	.208	.0195	062	.018	4.0	100 100	4.14	.268	.0372	083	035	3.9
	49	.012	.0113	038	.018	4.0		4.39	-359	.0358	071	.016	4.0		6.21	.383	.0588	110	043	3.9
	49	.080	.0121	042	.018	4.0		6.58	.505	.0633	074	.014	4.0		8.29	.496	.0880	137	051	3.8
	1.09	.115	.0133	045	.019	4.0		8.78	.666	.1050	087	.012	4.0		9.32	.550	.1052	150	054	3.8
	2.17	184	.0167	049	.018	4.0		10.95	.815	.1589	111	.011	4.0		3.32	.,,,,	.10)2	1)0	0)4	2.0
	4.31	.313	.0288	055	.016	4.0		10.9)	.01)	.1,09		.011	4.0	1.70	4:16	196	.0312	.024		4.0
	6.46	.452	.0531	058	.012	4.0	1.20	4.24	283	.0374	.024	005	4.0		-2.09	090	.0207	.001	008	4.0
	8.61	.581	.0881	059	.007	4.0	1.20	-2.13	127	.0228	008	011	4.0		-1.07	037	.0180	011	012	4.0
	10.77		.1356	063	.003	4.0		-1.10	046	.0193	025	014	3.9		54	009	.0173	016	014	4.0
		.717	.1909	070	001	4.0			007	.0193	023	014	3.9		.49	.047	.0175	029	019	3.9
	12.92	.963	.2531	073	004	4.0		56	.072	.0189	033	021	3.9	1	1.02	.075	.0184	035	021	3.9
				064	008	4.0	1			.0200	058	024	3.9		2.06	.129	.0219	046	025	3.9
	17.15	1.041	.3144					1.02	.112					100	4.13		.0343	069	033	
	18.19	1.066	.3446	059	014	4.0		2.07	.190	.0248	075	029	3.9		6.19	.234			042	3.9
								4.17	.346	.0416	109	038	3.9			-334	.0531	092		3.9
0.80	4.39	254	.0296	030	.022	4.1	1	6.27	.500	.0688	142	047	3.8		8.26	.432	.0785	114	049	3.8
	-2.20	099	.0157	038	.023	4.1		7.33	.577	.0863	151	052	3.8	200	10.32	.527	.1105	136	057	3.8
	-1.08	020	.0123	043	.023	4.1									11.36	-573	.1290	146	061	3.8
	50	.015	.0122	046	.024	4.1	1.30	4.22	262	.0374	.027	003	4.0							
	.56	.091	.0131	051	.024	4.1		-2.12	119	.0238	004	012	4.0	1.90	4.14	171	.0301	.017	0	4.0
	1.10	.126	.0145	054	.024	4.1	Mark Tolland	-1.10	047	.0204	020	016	3.9		-2.08	080	.0213	001	006	4.0
	2.19	.203	.0186	059	.024	4.1		56	011	.0195	028	018	3.9		-1.06	032	.0193	011	010	4.0
	4.37	.346	.0334	066	.022	4.1		.49	.062	.0198	044	022	3.9		54	009	.0188	015	013	4.0
	6.54	.486	.0597	067	.018	4.0		1.02	.097	.0209	051	024	3.9	1	.49	.040	.0189	025	017	4.0
	8.73	.636	.0985	076	.009	4.0	1000	2.06	.168	.0254	066	028	3.9	1	1.02	.064	.0196	030	019	3.9
	10,90	.778	.1504	089	001	4.0		4.16	.309	.0413	098	035	3.9		2.05	.110	.0224	039	024	3.9
	13.06	.914	.2123	101	010	4.0		6.24	.446	.0660	129	044	3.9		4.11	.201	.0329	057	032	3.9
	25,00	.,						7.29	.510	.0809	142	048	3.8		6.17	.290	.0494	076	041	3.9
0.90	4.41	263	.0312	030	.023	4.1		1.0	.,120				3.3		8.22	.376	.0718	095	050	3.8
0.90	-2.22	107	.0168	039	.022	4.1	1.50	4.18	226	.0333	.026	003	4.0		10.27	.458	.0996	113	058	3.8
	-1.09	023	.0133	045	.021	4.1	1.,00	-2.10	104	.0214	0	011	4.0		12.33	.540	.1333	131	066	3.8
				048	.020	4.1	100	-1.09	044	.0182	014	016	3.9		14.39	.619	.1729	148	072	3.8
	50	.016	.0129	048	.020	4.1	1900		011	.0102	022	017	3.9		14.39	.019	17/29	140	012	3.0
	200				1	1 1 2 1 1 1 1	3 / 19	55	.053	.0175	036	021	3.9			10.00		TOTAL T	MANA	
			A. 14. A.B.		LEW T	1940		49	.073	.0110	030	021	2.3							_

(c) Characteristics for wing-body-tail combination;  $\delta_n = 0^\circ$ 

М	α	$c_{\mathbf{L}}$	$c_D$	Cm	C <sub>h</sub>	8	М	α	C <sub>L</sub>	c <sub>D</sub>	Cm	Ch	8	М	α	$c_{\mathbf{L}}$	$c_{\mathbb{D}}$	Cm	Ch	8
.60	4.30	-0.274	0.0280	0.007	0.003	0.2	0.90	4.40	-0.327	0.0340	0.015	0.006	0.2	1.50	-0.51	-0.030	0.0159	0.003	0.001	0.
.00	-2.15	140	.0149	.002	.003	0.2	0.50	-2.21	163	.0166	.006	.006	0.2	2.,00	.50	.031	.0158	011	005	0.
	-1.06	069	.0115	002	.002	0.2		-1.11	084	.0122	0	.005	0.2		1.03	.064	.0165	018	007	0.
			.0108	005	.002	0.2		54	042	.0102	003	.008	0.2		2.07	.127	.0200	032	012	0
	55	036	.0104	009	.002	0.2		.52	.038	.0105	010	.009	0.2		4.16	.246	.0327	058	020	0
	1.06	.065	.0107	011	.003	0.2		1.08	.078	.0112	013	.008	0.2		6.23	.363	.0529	085	028	0
					.004	0.2		2.18		.0143	020	.008	0.2		8.31	.477	.0810	111	037	0
	2.13	.133	.0132	015				4.38	.159	.0295	020	.011	0.2		10.37	.583	.1157	136	045	0
	4.26	.262	.0227	022	.005	0.2		6.58	.321	.0584	032	.011	0.2		10.51	.,05	1000	130	04)	0
	6.41	.400	-0456	026	.007	0.2					-:066	.012	0.2	1.70	4.16	214	.0318	.041	.013	0
	8.57	.536	.0784	028	.009	0.2		8.77	.659	.1030	-:000	.012	0.2	2.10	-2.08	106	.0203	.018	.005	0
-53	9.63	-599	.0976	030	.010	0.2	1	1 00	270	0000	050	.007	0.2		-1.04	051	.0171	,006	.001	0
	10.71	.665	.1197	033	.011	0.2	1.20	4.22	319	.0383	.058		0.2		51	025	.0163	.001	001	0
	11.77	.731	.1445	036	.012	0.2		-2.11	161	.0219	.027	0			.50	.030	.0162	011	003	0
	12.85	.800	.1730	041	.013	0.2		-1.06	079	.0177	.010	0	0.2		1.03	.058	.0169	017	005	0
12	13.90	.855	.1995	044	.013	0.2		52	039	.0164	.002	001	0.2		2.07	.112	.0199	029	010	0
	14.97	.911	.2320	045	.013	0.2		.50	.037	.0160	015	003	0.2		4.14	.217	.0313	051	019	0
	16.03	.959	.2628	042	.013	0.2		1.04	.079	.0167	024	005	0.2		6.21	.318	.0491	073	027	0
	17.08	.993	.2920	039	.012	0.2		2.09	.159	.0205	042	009	0.2		8.28	.415	.0736	095	035	0
	18.10	1.018	.3206	040	.009	0.2		4.19	.317	.0356	076	016	0.1		10.35	.511	.1044	116	044	0
								6.29	.471	.0612	110	025	0.1		11.38	.562	.1226	127	048	0
80	4.36	303	.0339	.011	.004	0.2		8.39	.628	.0979	145	037	0.1		11.30	.502	.1220	121	040	10
	-2.18	151	.0154	.003	.002	0.2							-		1 1 1 2 2					
	-1.10	073	.0114	002	.003	0.2	1.30	4.19	290	.0378	.057	.013	0.2	1.90	4.13	186	.0303	.031	.014	0
	56	037	.0105	005	.003	0.2		-2.09	146	.0227	.026	.004	0.2		-2.07	092	.0204	.013	.006	0
	.52	.034	.0100	010	.004	0.2		-1.05	070	.0185	.010	0	0.2		-1.03	045	.0180	.004	.002	0
	1:07	.071	.0106	013	.005	0.2		52	035	.0170	.002	002	0.2	100000	50	023	.0173	0	0	0
	2.16	.143	.0132	018	.006	0.2		.51	.035	.0171	013	006	0.2		.48	.024	.0173	010	002	0
	4.33	.285	.0256	026	.008	0.2		1.04	.072	.0177	021	008	0.2	1	1.01	.048	.0178	014	005	0
	6.50	.428	.0496	030	.010	0.2		2.08	.145	.0214	037	012	0.2		2.05	.095	.0201	023	009	0
	8.68	.588	.0890	042	.012	0.2		4.17	.284	.0354	068	-,020	0.1	1	4.12	.184	.0295	042	018	0
	9.76	.655	.1108	050	.013	0.2		6.25	.420	.0582	099	028	0.1		6.17	.272	.0448	060	027	0
	10.84	.722	.1344	055	.014	0.2		8.33	.553	.0906	129	037	0.1		8.22	.358	.0661	078	035	0
	11.92	.796	.1638	064	.016	0.2		9.37	.615	.1096	143	041	0.1	100	10.28	.440	.0928	096	043	0
	13.00	.866	.1948	073	.018	0.2	1							12000	12.34	.522	.1255	112	051	0
	14.06	.924	.2258	084	.020	0.3	1.50	4.17	249	.0344	.050	.013	0.3		14.40	.598	.1632	128	058	0
	15.13	.980	.2591	094	.020	0.3	1	-2.09	126	.0209	.023	.004	0.2							
	8.19	.554	.0793	038	.012	0.2		-1.05	061	.0170	.009	0	0.2			1 8				1

TABLE II. - AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 WITH LEADING-EDGE CHORD EXTENSIONS AND AN ALL-MOVABLE HORIZONTAL TAIL - Continued

(d) Characteristics for wing-body-tail combination;  $\delta_n = -2^\circ$ 

M	α	CL	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	8	M	α	$C_{\mathbf{L}}$	$c_{\mathrm{D}}$	Cm	Ch	8
.60	4.32	-0.300	0.0297	0.021	-0.001	-1.6	0.90	-1.11	-0.101	0.0119	0.016	0	-1.6	1.50	-1.05	-0.075	0.0176	0.018	0.007	-1.
	-2.17	166	.0156	.016	0	-1.6		56	062	.0108	.012	001	-1.6		52	044	.0162	.011	.005	-1.
	-1.09	093	.0115	.013	.001	-1.6	0	.54	.022	.0101	.006	001	-1.6		.50	.020	.0157	003	.001	-1.
	54	060	.0105	.011	.001	-1.6	2	1.07	.056	.0105	.003	0	-1.6	100	1.03	.052	.0163	009	.001	-1
	.52	.010	.0098	.007	001	-1.6	Out -	2.18	.136	.0133	002	.002	-1.6	1	2.08	.114	.0195	023	003	-1
						-1.6		4.37	.294	.0273	012	.005	-1.6	C	4.15	.233	.0320	049	012	-1
	1.06	.042	.0103	.006	001				.456	0547	022	.005	-1.6		6.23	.349	.0517	075	021	-1
	2.12	.109	.0122	.002	001	-1.6		6.57	.626	.1001	047	.006	-1.6		8.30	.461	.0788	102	029	-1
	4.26	.240	.0212	006	0	-1.6	100	9.03						100	10.37	.568	.1133			
	6.42	.380	.0430	009	0	-1.6	600	9.86	.698	.1217	052	.009	-1.6					127	037	-1
	8.56	.512	.0752	010	.001	-1.6		10.96	.791	.1532	073	.014	-1.6	130	11.56	.629	.1365	141	042	-1
	9.64	.578	.0946	013	.002	-1.6			and the same	1	100			1000	1,33			40.00	1	1
	10.71	.641	.1159	015	.003	-1.6	1.20	4.21	339	.0403	.073	.018	-1.5	1.70	4.15	224	.0328	.049	.021	-1
	11.78	.705	.1398	018	.004	-1.6		-2.11	177	.0205	.041	.009	-1.6		-2.08	117	.0208	.026	.012	-1
	12.85	.776	.1681	023	.005	-1.6		-1.05	095	.0156	.023	.005	-1.6		-1.04	062	.0174	.014	.008	-1
	13.92	.835	.1967	026	.006	-1.6	D.X.	53	056	.0141	.015	.004	-1.6		51	034	.0164	.009	.007	-1
	14,98	.887	,2258	026	.007	-1.6		.50	.025	.0163	002	0	-1.6		.49	.019	.0159	003	.002	-1
	16.04	.935	.2566	023	.008	-1.6		1.04	.062	.0142	009	0	-1.6	1	1.03	.047	.0165	009	0	-1
	17.09	.971	.2855	019	.009	-1.6		2.09	.139	.0190	026	002	-1.6		2.07	.100	.0192	020	002	-1
	18.12	.999	.3144	020	.010	-1.6		4.19	.298	.0349		007	-1.6		4.14	.201	.0299	041	011	-1
	10.12	• 555	.3244	020	.010	-2.0		6.28	.453	.0600		013	-1.6		6.21	.303	.0472	063	021	-1
0.80	1, 20	200	0205	.028	0	-1.6		8.38	.611	.0933		023	-1.7		8.28	.401	.0710	085	029	-1
0.00	4.38	329	.0325		.001			8.99	.661	.1065		027	-1.7		10.34	.492	.1009	105	037	-1
	-2.20	177	.0162	.021		-1.6		0.99	.001	.100)	143	021	7.1		12.41	.582	.1373	125	045	-1
	-1.11	098	.0116	.015	001	-1.6		1 20	310	.0401	.069	.019	-1.5	120 - 3	10.41	. ,02	*7212	12)	04)	-
	55	061	.0104	.013	001	-1.6	1.30	4.19		.0240		.019	-1.6	1.90	4.13	193	.0309	.038	.021	-1
	-53	.015	.0098	.007	0	-1.6		-2.10	163					1.90						
	1.09	.051	.0102	.005	0	-1.6	1000	-1.05	088	.0194		.008	-1.6		-2.07	100	.0209	.019	.012	-1
	2.15	.124	.0125	0	0	-1.6		52	052	.0181		.006	-1.6		-1.03	052	.0182	.010	.008	
	4.33	.269	.0244	010	0	-1.6		.50	.022	.0171		.001	-1.6	1	50	029	.0174	.005	.006	
	6.51	.413	.0477	012	.001	-1.6		1.04	.055	.0176		0	-1.6		.49	.017	.0170	004	.002	-1
	8.68	.562	.0853	023	.003	-1.6		2.08	.127	.0212		002	-1.6		1.02	.041	.017,4		0	-
	9.76	.630	.1071	029	.004	-1.6		4.17	.267	.0349		011	-1.6		2.06	.087	.0195	017	003	
	10.85	.704	.1450	036	.006	-1.6		6.26	.403	.0573		019			4.12	.176	.0287	034	013	-:
	11.94	.778	.1604	043	.009	-1.6		8.34	-537	.0892		028			6.18	.263	.0435	052	022	-
	13.01	.841	.1894	051	.012	-1.6		10.02	.639	.1209	140	034	-1.7		8.23	.349	.0647	069	031	-1
	-			1					1000					1	10.29	.430			039	
0.90	3.52	354	0133	.035	.003	-1.6	1.50	4.17	265	.0360	.060	.019	-1.5		12.35	.510		103	046	
,0	-2.22	188			.001			-2.09	140			.011			14.40	.587			052	

(e) Characteristics for wing-body-tail combination;  $\delta_n = -4^{\circ}$ 

М	α	CL	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	8	M	α	CL	CD	Cm	Ch	8
0:60	4.32	-0.323	0.0324	0.043	-0.010	-3.8	0.90	-2.23	-0.220	0.0204	0.054	0	-3.8	1.30	4.17	0.251	0.0341	-0.038	0	-3.
	-2.17	187	.0172	.037	009	-3.8		-1.12	134	.0142	.046	001	-3.8		6.26	.387	.0555	068	006	-3
	-1.10	118	.0127	.034	008	-3.8		57	093	.0126	.043	001	-3.8		8.34		.0859	098	014	-3
	55	081	.0116	.032	008	-3.8		.49	013	.0114	.037	001	-3.8		10.19	.517	.1204	123	022	-3
	.47	015	.0104	.028	007	-3.8		1.08	.028	.0114	.031	004	-3.8				Carlo Carlo			1
	1.04	.017	.0106	.026	006	-3.8		2.20	.111	.0138	.024	004	-3.8	1.50	4.16	274	.0373	.074	.030	-3
	2.13	.086	.0121	.022	004	-3.8		4.37	.269	.0267	.011	003	-3.8	21,70	-2.08	148	.0227	.046	.023	-3
	4.25	.215	.0202	.014	002	-3.8		6.57	.433	.0532	001	001	-3.8		-1.03	083	.0183	.031	.018	-3
	6.38	.350	.0398	.011	.001	-3.8		8.77	.600	.0947	021	0	-3.8		51	051	.0169	.024	.016	-3
	8.56	.483	.0716	.010	.001	-3.8		10.95	.758	.1484	047	.007	-3.8	1000	.53	.013	.0163	.010	.012	-3
	10.68	.614	.1113	.005	002	-3.8		20.77	1,70	12.01	70.1	1001	3.0		1.04	440.	:0168	.003	.010	-3
	12.82	.749	.1627	003	0	-3.8	1.20	4.20	352	.0416	.094	.034	-3.7		2.09	.103	.0198	010	.006	<del>-3</del>
	14.94	.856	.2181	006	.003	-3.8	1.50	-2.09	197	.0244	.062	.024	-3.7		4.17	.220			0.000	
	17.04	.937	.2752	.001	.004	-3.8	100	-1.04	111	.0191	.044	.020	-3.7		6.25	.335	.0313	035 061	008	-3 -3
	18.07	.963	.3022	.002	.005	-3.8	1 75 18	52	072	.0177	.036	.018	-3.7		8.32	.448	.0770	087		
	20.01	.903	.3022	3002	.00)	-5.0		.54	.008	.0168	.019	.014	-3.8		10.39				016	-3
.80	-4.39	356	.0356	.054	014	-3.8		1.08	.049	.0174	.011	.011	-3.8		11.14	•553	.1105	111	025	-3
1.OU	-2.21	205	.0183	.046				2.11	.122	.0204	006	.006	-3.8		11.14	.591	.1245	120	028	-3
	-1.12		.0129	.040	013	-3.8		4.20	.277	.0340	040	001								
		129			011	-3.8		6.30	.432		074		-3.8	1.70	4.14	234	.0344	.060	.031	-3
	57	090	.0117	.038	011	-3.8	1	8.40		.0577		001	-3.8		-2.07	127	.0220	.037	.022	-3
		016	.0105	.033	009	-3.8			•589	.0931	110	008	-3.8		-1.03	069	.0182	.024	.017	-3
	2.18	.097	.0126	.024	005	-3.8	1	8.98	.635	.1050	120	012	-3.8		50	042	.0171	.019	.015	-3
	1.07	.021	.0108	.030	007	-3.8				2126	-00				-53	.015	.0164	.006	.011	-3
	4.32	.240	.0232	.014	002	-3.8	1.30	4.18	319	.0416	.088	.027	-3.7		1.03	.040	.0169	.001	.009	-3
	6.49	.381	.0451	.010	0	-3.8	1	-2.09	178	.0255	.057	.023	-3.7		2.08	.093	.0194	010	.005	-3
	8.68	.536	.0821	0	.001	-3.8	1	-1.03	099	.0206	.039	.018	-3.7		4.15	.194	.0297	031	001	-3
	10.83	.672	.1272.	013	001	-3.8		52	063	.0191	.031	.016	-3.8		6.22	.294	.0464	053	010	-3
	13.00	.810	.1832	029	.001	-3.8	1	.54	.011	.0181	.015	.012	-3.8		8.28	.392	.0696	074	018	-3
			-1					1.07	.047	.0185	.008	.010	-3.8	1	10.35	.482	.0989	094	026	-3
0.90	4.43	387	.0405	.067	.007	-3.8		2.09	.114	.0216	007	.007	-3.8		12.42	.580	.1365	114	035	-3

TABLE II. - AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 WITH LEADING-EDGE CHORD EXTENSIONS AND AN ALL-MOVABLE HORIZONTAL TAIL - Continued

(f) Characteristics for wing-body-tail combination;  $\delta_n = -8^{\circ}$ 

M .	- α	CL	CD	Cm	Ch	8	М	α	CL	CD	Cm	ch	8	М	α	CL	CD	Cm	Ch	8
0.60	4.34	-0.363	0.0410	0.070	0.009	-7.6	0.90	1.01	-0.032	0.0164	0.079	0.012	-7.8	1.50	1.07	0.021	0.0184	0.026	0.028	-7.
	-2.22	231	.0240	.069	.004	-7.7		2.18	.053	.0176	.073	.010	-7.8		2.13	.082	_0209	.013	.023	-7.
	-1.12	163	.0185	.067	0	-7.8		4.39	.219	.0283	.061	.005	-7.8		4.17	.198	.0311	014	.014	-7.
	59	132	.0169	.066	0	-7.8		6.59	.386	.0532	.049	.001	-7.8		6.25	.313	.0488	039	.005	-7
	.49	066	.0143	.064	004	-7.9		8.76	.551	.0919	.029	.004	-7.8	100	8.32	.423	.0739	063	0	-7
	1.03	034	.0136	.062	005	-7.9		10.94	.710	.1435	.002	.012	-7.8		10.39	-528	.1063	087	008	-7
	2.09	.033	.0139	.058	009	-8.0		20.7	1,20	12137			1.0	1	12.25	.619	.1414	108	016	-7
153	4.25	.167	.0200	.051	010	-8.0	1.20	4.18	385	.0483	.125	.056	-7.6							
	6.40	.303	.0374	.046	009	-8.0		-2.08	229	.0295	.094	.047	-7.6	1.70	4.13	253	.0384	.079	.047	-7
	8.53	.434	.0650	.044	007	-79	0.25	-1.03	148	.0237	.076	.043	-7.7		-2.06	143	.0249	.055	.038	-7
	10.65	.570	.1059	.038	006	-7.9		50	106	.0219	.068	.041	-7.7		-1.02	088	.0208	.043	.033	-7
	12.79	.702	.1544	.030	004	-7.9		.51	030	.0203	.053	.037	-7.7		50	060	.0194	.037	.031	-7
	14.90	.807	.2075	.026	002	-7.8		1.08	.010	.0203	.045	.035	-7.7		.50	004	.0182	.025	.027	-7
	17.00	.889	.2628	.034	001	-7.8	1 3	2.15	.089	.0226	.028	.029	-7.7	1	1.06	.023	.0184	.019	.024	-7
	18.05	.921	.2915	.035	0	-7.8		4.22	.242	.0346	007	.018	-7.7		2.12	.077	.0205	.008	.020	-7
	20.0)	. 722		.03)	0	1.0		6.31	-393	.0567	038	.010	-7.8		4.15	.175	.0298	013	.011	-7
.80	4.40	397	.0453	.086	013	-7.8		8.41	.551	.0898	074	0	-7.8		6.22	.275	.0455	034	.002	-7
	-2.23	253	.0262	.082	016	-7.8	1100	9.73	.654	.1175	095	002	-7.8		8.29	.370	.0676	054	004	-7
	-1.14	177	.0197	.079	017	-7.8		2.12			.0))	-1002	1.0		10.35	.462	.0961	074	012	-7
	59	141	.0176	.076	017	-7.8	1.30	4.16	347	.0473	.112	.045	-7.7	1	12.42	.551	.1309	093	021	-7
	.44	070	.0152	.072	018	-7.8	2.50	-2.07	205	.0300	.083	.037	-7.7		13.50	.597	.1512	102	025	-7
	.99	035	.0146	.070	018	-7.8	0.00	-1.02	131	.0247	.067	.034	-7.7							
	2.13	.040	.0151	.065	018	-7.8	19.	51	093	.0227	.059	.033	-7.7	1.90	4.11	217	.0359	.060	.043	-7
	4.32	.187	.0234	.056	016	-7.8		.56	022	.0212	.044	.030	-7.7		-2.06	121	.0245	.042	.034	-7
	6.50	.329	.0430	.051	016	-7.8	137	1.08	.014	.0212	.037	.029	-7.7		-1.01	073	.0211	.033	.029	-7
	8.64	.477	.0745	.040	014	-7.8		2.14	.085	.0237	.022	.025	-7.7	1 1 2 3	49	050	.0200	.028	.026	-7
	10.81	.623	.1191	.026	011	-7.8		4.19	.222	.0345	009	.018	-7.7		.50	002	.0192	.020	.055	-7
	12.96	.756	.1735	.008	005	-7.8		6.27	.355	.0541	039	.010	-7.8	1	1.05	.020	.0194	.015	.019	-7
	12.90	. (50	*1(2)	,000	005	-1.0		8.42	.488	.0832	069	.002	-7.8		2.10	.067	.0212	.006	.015	-7
.90	4.45	431	.0506	.098	.015	-7.8		10.52	.609	.1205		.002	-7.8		4.13	.151	.0290	011	.007	-7
.90	-2.24	431	.0287	.090	.015	-7.8	The same	10.52	.009	.1502	095	.004	-1.8		6.18	.238	.0429	027	002	-7
	-1.14	187	.0219	.088	.014	-7.8	1.50	4.14	301	.0428	.100	.043	-7.7	0. 49	8.24	.321	.0625	043	012	-7
		146	.0196	.086	.013	-7.8	1.00	-2.06	176	.0268	.071				10.29	.402	.0873	059	019	-7
20.	59	071	.0169	.081	,010	-7.8		-1.02	109	.0200		.038	-7.7	1 4 1 1 1	12.35	.480	.1175	071	026	-7
3334	•45	0/1	.0109	*001	*010	-1.0	1 5 8 8	50	077		.055	.034	-7.7	1 1 5 1	14.40	.559	.1535	084	032	-7
DE.				1		100		50		.0197		.033	-7.7	1 3 3 1	27.40	.)))	. 200)	.304	032	-1.
					1			.50	012	.0183	.033	.030	-7.7				CAN STREET		100000	

(g) Characteristics for wing-body-tail combination;  $\delta_n = -12^\circ$ 

M	α	$c_{\rm L}$	CD	Cm	Ch	δ	М	α	CL	CD	Cm	Ch	δ	М	α	$c_{\rm L}$	CD	Cm	Ch	8
0.60	-4.33	-0.362	0.0477	0.075	0.030	-11.7	0.90	1.07	-0.035	0.0225	0.087	0.028	-11.7	1.50	0.51	-0.037	-0.0260	0.058	0.043	-11.6
1	-2.19	233	.0311	.076	.027	-11.8		2.14	.026	.0237	.094	.016	-11.8	1.50	1.07	005	.0258	.051	.042	-11.7
	-1.11	168	.0263	.076	.027	-11.8	777	4.36	.187	.0333	.087	.015	-11.8	1901	2.14	.058	.0274	.037	.039	-11.7
1	59	138	.0244	.076	.027	-11.8	- Maria	6.56	.350	.0564	.077	.011	-11.8		4.19	.173	.0356	.010	.033	-11.7
	.47	077	.0219	.076	.025	-11.8	735	8.75	.508	.0928	.062	.007	-11.8	1	6.27	.288	.0518	017	.023	-11.7
	1.03	049	.0215	.077	.024	-11.8	11524	10.89	.659	.1424	.041	.025	-11.7		8.34	.399	.0755	041	.014	-11.8
	2.08	.015	.0210	.076	.021	-11.8	1								10.41	.503	.1064	065	.006	-11.8
	4.25	.139	.0253	.074	.014	-11.8	1.20	-4.17	406	.0586	.150	.079	-11.5		77.7	.,00				
	6.39	.273	.0404	.073	.007	-11.8		-2.06	253	.0391	.122	.072	-11.6	1.70	-4.12	275	.0475	.101	.060	-11.6
	8.53	.399	.0664	.075	.002	-11.8		-1.01	175	.0329	.106	.068	-11.6		-2.05	165	.0325	.076	.055	-11.6
1000	10.67	.530	.1024	.072	0	-11.8	100	48	136	.0308	.098	.066	-11.6		-1.01	108	.0277	.063	.050	-11.6
177	12.87	.658	.1486	.066	006	-11.8	1700	.51	060	.0286	.083	.062	-11.6	7 990	49	081	.0261	.057	.048	-11.6
1000	14.89	.763	.2017	.061	008	-11.8	- 37	1.05	020	.0283	.075	.059	-11.6		.50	026	.0244	.045	.043	-11.6
	17.00	.843	.2544	.069	009	-11.8	10000	2.17	.061	.0299	.058	.052	-11.6	100	1.06	.001	.0243	.038	.040	-11.7
	18.02	.866	.2781	.071	009	-11.8	1	4.27	.215	.0404	.024	.044	-11.7		2.13	.057	.0257	.027	.035	-11.7
100	100				689	100		6.34	.364	.0607	007	.035	-11.7		4.17	.156	.0337	.005	.025	-11.7
0.80	-4.39	369	.0484	.070	.029	-11.7		8.44	.516	.0921	039	.024	-11.7		6.24	.256	.0486	016	.016	-11.7
1 8 1	-2.21	231	.0307	.071	.029	-11.7	1000	9.49	.601	.1131	057	.020	-11.7		8.31	.351	.0698	035	.007	-11.8
10195	-1.12	160	.0252	.071	.028	-11.7	727	ALC: NO							10.37	.441	.0969	054	.001	-11.8
1000	58	126	.0234	.071	.028	-11.7	1.30	-4.15	366	.0562	.135	.065	-11.6		12.44	.531	.1306	073	007	-11.8
	.45	063	.0215	.072	.026	-11.7	1119 9	-2.06	227	.0385	.106	.056	-11.6			1				
	1.00	030	.0208	.071	.025	-11.7		-1.01	152	.0328	.091	.053	-11.6	1.90	-4.10	234	.0426	.078	.057	-11.6
	2.14	.039	.0213	.071	.023	-11.7		48	118	.0309	.084	.051	-11.6		-2.04	139	.0323	.058	.047	-11.7
	4.33	.176	.0289	.069	.019	-11.8		.57	048	.0288	.070	.047	-11.6		-1.01	090	.0263	.048	.042	-11.7
	6.50	.311	.0477	.071	.012	-11.8	100	1.11	012	.0286	.063	.045	-11.7		50	067	.0249	.044	.039	-11.7
	8.67	.453	.0783	.066	.003	-11.8		2.18	.060	.0304	.048	.040	-11.7		.49	020	.0235	.035	.034	-11.7
1	10.83	.583	.1191	.057	005	-11.8		4.24	.193	.0398	.018	.034	-11.7		1.04	.002	.0236	.031	.032	-11.7
	12.95	.706	.1672	.047	018	-11.8		6.29	.328	.0578	010	.029	-11.7		2.09	.050	.0249	.022	.027	-11.7
1.000	15.08	.823	.2253	.028	015	-11.8		8.38	.456	.0850	039	.023	-11.7		4.13	.136	.0322	.005	.018	-11.7
1.60	100							10.49	.578	.1213	066	.014	-11.8		6.19	.222	.0453	011	.009	-11.8
0.90	-4.41	406	.0531	.088	.035	-11.7			THE STATE OF						8.24	.306	.0643	027	001	-11.8
	-2.23	247	.0322	.080	.032	-11.7	1.50	-4.14	317	.0518	.118	.053	-11.6		10.29	.384	.0879	042	005	-11.8
	-1.13	167	.0259	.077	.031	-11.7		-2.05	197	.0355	.094	.049	-11.6	74 (1)	12.35	.462	.1174	055	014	-11.9
	58	130	.0236	.076	.030	-11.7		-1.01	132	.0300	.080	.048	-11.6		14.40	.541	.1518	070	021	-11.9
	.53	072	.0228	.087	.030	-11.7		49	101	.0281	.073	.047	-11.6		16.46	.614	.1923	083	027	-11.9

TABLE II.- AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 WITH LEADING-EDGE CHORD EXTENSIONS AND AN ALL-MOVABLE HORIZONTAL TAIL - Continued

(h) Characteristics for wing-body-tail combination;  $\delta_n = -16^{\circ}$ 

М	α	CL	CD	Cm	Ch	δ	М	α	$c_{\mathbf{L}}$	CD	Cm	Ch	8	М	α	CL	CD	Cm	Ch	δ
0.60	-4.32	-0.343	0.0505	0.065	0.030	-15.6	0.90	2.19	0.060	0.0285	0.071	0.035	-15.6	1.50	1.03	-0.031	0.0326	0.072	0.056	-15.5
	-2.18	212	.0344	.065	.030	-15.6		4.39	.214	.0359	.066	.034	-15.6		2.14	.033	.0340	.059	.054	-15.5
	-1.10	147	.0297	.065	.030	-15.6		6.59	.372	.0634	.060	.033	-15.6		4.23	.152	.0418	.033	.050	-15.5
	57	117	.0283	.065	.030	-15.6		8.79	.525	.1004	.050	.032	-15.6		6.27	.267	.0564	.006	.040	-15.6
	.44	058	.0266	.066	.030	-15.6		10.92	.641	.1490	.055	.022	-15.6		8.34	.377	.0788	~.019	.030	-15.6
	.98	029	.0259	.066	.030	-15.6			THE STATE OF						10.41	.481	.1081	042	.021	-15.6
	2.10	.031	.0262	.067	.031	-15.6	1.20	-4.15	421	.0694	.165	.098	-15.4	180	12.48	.582	.1449	064	.014	-15.7
	4.25	.146	.0321	.073	.032	-15.6		-2.05	273	.0489	.139	.092	-15.4		100			- 1		
	6.40	.267	.0483	.080	.028	-15.7		-1.00	195	.0423	.126	.089	-15.4	1.70	-4.11	292	.0565	.117	.064	-15.5
	8.52	.388	.0724	.084	.024	-15.7		48	158	.0398	.119	.088	-15.4		-2.04	186	.0409	.096	.065	-15.5
	10.66	.515	.1079	.085	.019	-15.7		.51	085	.0371	.105	.085	-15.4		-1.00	129	.0351	.082	.065	-15.
	12.80	.635	.1525	.083	.013	-15.7		1.05	048	.0367	.099	.083	-15.4		48	102	.0331	.076	.064	-15.5
	14.93	.736	.2022	.084	.008	-15.7		2.16	.033	.0376	.082	.081	-15.4		.50	046	.0324	.063	.061	-15.5
	17.02	.806	.2517	.098	.005	-15.7		4.28	.186	.0468	.050	.072	-15.5		1.03	019	.0305	.057	.059	-15.5
	18.04	.824	.2730	.104	0	-15.7		6.34	•337	.0658	.019	.059	-15.5		2.13	.037	.0313	.045	.054	-15.5
	100							8.44	.491	.0959	013	.047	-15.5		4.21	.139	.0383	.024	.042	-15.6
0.80	-4.39	365	.0529	.071	.031	-15.6		10.56	.638	.1378	030	.043	-15.6		6.25	.236	.0518	.002	.031	-15.6
	-2.21	226	.0354	.070	.030	-15.6						1			8.31	.331	.0718	017	.021	-15.6
	-1.12	152	.0299	.069	.030	-15.6	1.30	-4.14	387	.0689	.153	.087	-15.4		10.38	.421	.0980	035	.012	-15.7
	57	119	.0282	.068	.030	-15.6		-2.05	249	.0497	.127	.080	-15.4		12.44	.508	.1300	053	.004	-15.7
	.46	052	.0263	.067	.029	-15.6		-1.00	177	.0433	.112	.077	-15.5		14.51	.592	.1680	070	002	-15.
	1.01	019	.0261	.067	.029	-15.6		47	142	.0410	.106	.075	-15.5			15,410				
	2.15	.050	.0267	.066	.029	-15.6		.51	073	.0382	.091	.071	-15.5	1.90	-4.09	-,250	.0509	.093	.074	-15.5
	4.34	.185	.0350	.065	.030	-15.6		1.03	037	.0375	.084	.069	-15.5		-2.04	156	.0376	.074	.065	-15.5
	6.51	.318	.0542	.069	.030	-15.6		2.15	.035	.0386	.069	.063	-15.5		-1.01	108	.0332	.064	.059	-15.5
	8.69	.455	.0852	.067	.027	15.6		4.24	.171	.0471	.040	.055	-15.5		50	085	.0317	.060	.056	-15.5
	10.85	.580	.1254	.064	.02.4	-15.6		6.29	.302	.0639	.013	.043	-15.6		.49	038	.0299	.051	.050	-15.5
	12.96	.697	.1732	.057	.016	-15.7		8.38	.429	.0900	014	.036	-15.6	96.11	1.02	015	.0298	.046	.047	-15.5
	15.08	.793	.2264	.051	002	-15.7		10.45	.548	.1247	037	.034	-15.6		2.11	.036	.0307	.038	.042	-15.6
				-01				12.10	.633	.1567	054	.029	-15.6	100	4.17	.123	.0375	.021	.030	-15.6
0.90	-4.43	397	.0610	.084	.037	-15.6					1			1000	6.20	.207	.0497	.004	.020	-15.6
	-2.23	246	.0388	.082	.039	-15.6	1.50	-4.12	334	.0610	.134	.069	-15.5	100	8.25	.290	.0678	011	.011	-15.7
	-1.12	163	.0315	.078	.037	-15.6		-2.04	217	.0431	.111	.063	-15.5		10.31	.370	.0912	025	.003	-15.7
	58	126	.0299	.076	.037	-15.6		-1.00	154	.0377	098	.061	-15.5		12.36	.447	.1203	039	001	-15.7
	.47	053	.0276	.074	.036	-15.6		48	122	.0375	.091	.060	-15.5	Arms	14.42	.521	.1539	052	007	-15.7
1	1.03	016	.0275	.072	.035	-15.6		.50	061	.0330	.078	.057	-15.5		16.47	.595	.1929	065	012	-15.7

(i) Characteristics for wing-body-tail combination;  $\delta_n = -20^{\circ}$ 

М	α	C <sub>L</sub>	$c_{\mathrm{D}}$	Cm	Ch	8	М	α	$c_{\rm L}$	$c_D$	Cm	Ch	δ	М	α	CL	$c_D$	Cm	Ch	8
0.60	-4.32	-0.342	0.0554	0.067	0.029	-19.7	0.90	1.03	-0.021	0.0339	0.079	0.044	-19.7	1.50	1.04	-0.050	0.0431	0.090	0.072	-19.5
	-2.18	216	.0405	.068	.029	-19.7		2.18	.054	.0349	.075	.040	-19.7		2.14	.011	.0438	.077	.067	-19.6
133	-1.11	150	.0356	.068	.028	-19.7		4.39	.207	.0452	.070	.038	-19.7		4.25	.129	.0508	.053	.063	-19.6
	57	120	.0341	.068	.028	-19.7		6.59	.370	.0702	.064	.038	-19.7		6.33	.244	.0647	.029		-19.6
	.45	060	.0322	.068	.027	-19.7		8.79	.534	.1101	.048	.038	-19.7		8.37	.352	.0854	.004	.058	-19.6
120	.99	032	.0320	.069		-19.7	10.4	10.92	.665	.1555	.031	.037	-19.7		10.44	.456	.1137	019	.046	-19.6
	2.10	.028	.0327	.068	.027	-19.7					111		7	100	12.51	-557	.1494	041	.035	-19.7
	4.26	.149	.0371	.069	.028	-19.7	1.20	-2.04	284	.0619	.153	.106	-19.4	1000					2 - 175	
	6.40	.274	.0535	.072	.030	-19.7	43	99	211	.0554	.141		-19.4	1.70	-4.11	303	.0663	.130	.073	-19.5
HI.	8.55	.399	.0799	.078	.031	-19.7	( -	47	173	.0527	.134	.101	-19.4		-2.03	202	.0515	.112		-19.6
-	10.68	.515	.1145	.083	.030	-19.7	100	.52	102	.0486	.122	.098	-19.4		99	149	.0461	.102		-19.6
	12.82	.633	.1596	.085	.030	-19.7		1.05	066	.0477	.115	.096	-19.4		47	122	.0440	.096		-19.6
	14.92	.710	.2047	.091	.027	-19.7		2.16	.011	.0483	.100	.093	-19.4		.51	066	.0411	.083	.068	
	17.03	.789	.2573	.110	.024	-19.8		4.28	.162	.0567	.072	.087	-19.4		1.03	040	.0405	.077		-19.6
	18.06	.802	.2777	.119	.020	-19.8		6.38	.315	.0759	.043	.083	-19.4	3 49.73	2.13	.015	.0408	.066		-19.6
5.70								8.45	.465	.1042	.012	.079	-19.4	1000	4.22	.118	.0468	-044	.061	-19.6
0.80	-4.38	371	.0594	.076	.036	-19.7		10.57	.610	.1449	001	.075	-19.5		6.30	.218	.0597	.022	.052	-19.6
	-2.21	232	.0422	.075	.035	-19.7		11.33	.654	.1610	001	.073	-19.5		8.33	.311	.0784	.003	.042	-19.7
	-1.12	157	.0361	.073	.034	-19.7	100							1300	10.40	.402	.1037	016	.030	-19.7
150	57	122	.0344	.072	.034	-19.7	1.30	-2.04	264	.0605	.142	.095	-19.4		12.47	.489	.1352	033	.020	-19.7
	.46	057	.0326	.071	.032	-19.7		-1.00	104	.0535	.129	.092	-19.4		14.54	-573	.1726	049	.012	-19.8
	1.01	024	.0320	.070	.031	-19.7		47	159	.0507	.123	.091	-19.4	130			A North		1975	
92.3	2.15	.044	.0327	.069	:030	-19.7		.51	091	.0477	.110	.089	-19.4	1.90	-4.09	267	.0624	.112	.073	-19.6
	4.33	.183	.0409	.067		-19.7		1.04	057	.0468	.103	.087	-19.4		-2.03	172	.0476	.093	.081	-19.5
The s	6.50	.317	.0599	.068	.030	-19.7		2.07	.018	.0463	.086	.085	-19.4		-1.00	124	.0428	.082	.079	-19.5
	8.67	.455	.0908	.065	.030	-19.7	1 1 10	4.26	.150	.0551	.061	.078	-19.4	M. Wei	48	101	.0411	.078	.077	-19.5
100	10.83	.579	.1308	.060	.030	-19.7		6.35	.284	.0716	.033	.070	-19.5		.50	054	.0388	.068	.071	
	12.94	.696	.1796	.055	.030	-19.7		8.40	.409	.0967	.008	.063	-19.5	Sales V	1.02	031	.0382	.064	.068	
	15.06	.785	.2310	.054	.027	-19.7		10.48	.527	.1305	014	.054	-19.5		2.10	.016	.0385	.054	.063	-19.6
16	-	100			1			12.56	.631	.1711	032	.046	-19.6		4.19	.103	.0443	.037	.053	-19.6
0.90	-4.42	403	.0653	.091	.045	-19.7								. 100	6.25	.189	.0562	.021	.044	-19.7
	-2.22	247	.0446	.086		-19.7	1.50	-4.12	346	.0715	.148	.081	-19.5	111	8.27	.270	.0735	.006	.032	-19.7
-16	-1.12	168	.0382	.084		-19.7		-2.04	233	.0547	.127		-19.5		10.33	.348	.0959	008	.022	-19.7
	58	132	.0362	.082		-19.7		99	172	.0487	.116		-19.5	1	12.39	.424	.1238	021	.013	-19.8
	.47	059	.0343	.081		-19.7		43	141	.0451	.110	.076	-19.5		14.45	.499	.1574	033	.005	-19.8
1		1	3.3	,,,,,				.51	080	.0433	.097		-19.5		16.51	-573	.1961	045	001	-19.8
		77	1 1 1/4		No.					7 3 7					137			5	NAC	A

TABLE II. - AERODYNAMIC CHARACTERISTICS OF A MODEL EMPLOYING A TRIANGULAR WING OF ASPECT RATIO 3 WITH LEADING-EDGE CHORD EXTENSIONS AND AN ALL-MOVABLE HORIZONTAL TAIL - Concluded

(j) Characteristics for wing-body-tail combination;  $\delta_n = -24^{\circ}$ 

M	α	CL	CD	Cm	Ch	8 .	М	α	CL	$c_{D}$	Cm	Ch	8	М	α	CL	$c_{\mathrm{D}}$	Cm	Ch	δ
0.60	-4.32	-0.343	0.0616	0.069	0.029	-23.7	0.90	-4.42	-0.409	0.0742	0.097	0.053	-23.7	1.50	2.14	-0.002	0.0550	0.092	0.086	-23.
,,,,,	-2.18	218	.0467	.070	.028	-23.7		-2.22	251	.0530	.091	.053	-23.7		4.24	.113	.0611	.067	.083	-23.
	-1.11	151	.0413	.070	.028	-23.7	- N	-1.12	175	.0467	.089	.054	-23.7		6.32	.225	.0747	.045	.075	-23.
	57	121	.0399	.070		-23.7		58	139	.0447	.088	.053	-23.7		8.36	.330	.0950	.023	.069	
	.45	061	.0380	.070		-23.7		.46	068	.0421	.087	.053	-23.7		10.44	.432	.1224	.002	.083	
	.99	031	.0375	.070		-23.7		1.02	031	.0413	.085	.053	-23.7		12.51	.532	.1565	019	.068	-23
	2.10	.029	.0375	.069	.028	-23.7	100	2.17	.046	.0424	.082		-23.7					-31	1000	100
	4.26	.1.53	.0431	.069		-23.7		4.38	.199	.0524	.077		-23.7	1.70	-4.10	313	.0774	.138	.084	
	6.40	.279	.0595	.071	.029	-23.7		6.58	.361	.0765	.070		-23.7		-2.02	214	.0627	.123	.082	
	10.68	.526	.1211	.076		-23.7		8.78	.525	.1153	.053		-23.7		99	162	.0575	.114	.081	
	12.82	.645	.1663	.075	.035	-23.7		10.89	.650.	.1578	.031	.040	-23.7		47	136	.0555	.109	.079	
	14.93	.739	.2164	.081		-23.7									.51	084	.0530	.099	.077	
	17.02	.798	.2648	.102	.041	-23.7	1.30	-3.80	382	.0880	.170		-23.4		1.03	057	.0524	.093	.076	
	18.05	.808	.2859	.116	.038	-23.7		-2.04	271	.0730	.152		-23.4		2.12	004	.0525	.083	.073	
	-						- 10	99	205	.0667	.141		-23.4		4.22	.096	.0579	.063	.072	
0.80	-4.38	373	.0665	.080	.038	-23.7		46	170	.0642	.135		-23.4		6.29	.198	.0695	.042	.073	
	-2.21	234	.0492	.079	.038	-23.7		-52	104	.0611	.123		-23.4		8.33	.295	.0868	.019	.064	
	-1.12	162	.0433	.079	.038	-23.7	lud 8	1.05	072	.0601	.117		-23.5		10.39	-386	.1111	001	.054	
	58	128	.0414	.078	.038	-23.7		2.15	002	.0600	.104		-23.5	1	12.45	.475		019	.044	
	.45	063	.0393	.077	.038	-23.7		4.27	.129	.0667	.077		-23.5		14.52	.560	.1786	036	.034	
	1.01	030	.0388	.076	.037	-23.7		6.36	.263	.0825	.051		-23.5		16.58	.642	.2209	053	.022	-53
	2.14	.039	.0390	.074	.037	-23.7		8.41	.386	.1062	.027		-23.5					-0-		
	4.33	.176	.0465	.071	.037	-23.7		10.50	.501	.1386	.004		-23.6	1.90	1.02	052	.0500	.085	.079	
	6.50	.311	.0652	.073	.038	-23.7		12.58	.608	.1788	014	.076	-23.5		2.11	001	.0488	.072	.076	
700	8.67	.451	.0962	.068	.038	-23.7									4.18	.091	.0531	.053	.066	
	10.83	.582	.1373	.060	.034	-23.7	1.50	-4.11	354	.0828	.155		-23.5		6.24	.178	.0641	.036	.055	
- 3	12.94	.700	.1857	.051	.032	-23.7		-2.03	241	.0659	.136		-23.5		8.26	.261	:0809	.018	.044	
	15.07	.799	.2403	.045		-23.7		99	182	.0601	.126		-23.5		10.31	.342	.1035	.003	.034	
	-,,,,,,	177	1					47	152	.0577	.121	.095	-23.5		12.36	.419	.1311	012	.026	
	200			1800		1000		-52	093	.0548	.110	.092	-23.5		14.41	.494	.1638	025	.020	
Rich				130				1.04	065	.0543	.104	.091	-23.5		16.47	.571		037	.013	
1	TE SEN			1	-	1									17.50	.607	.2234	043	.011	-23

32.37

+1.98 +3.90+ -7.80 -

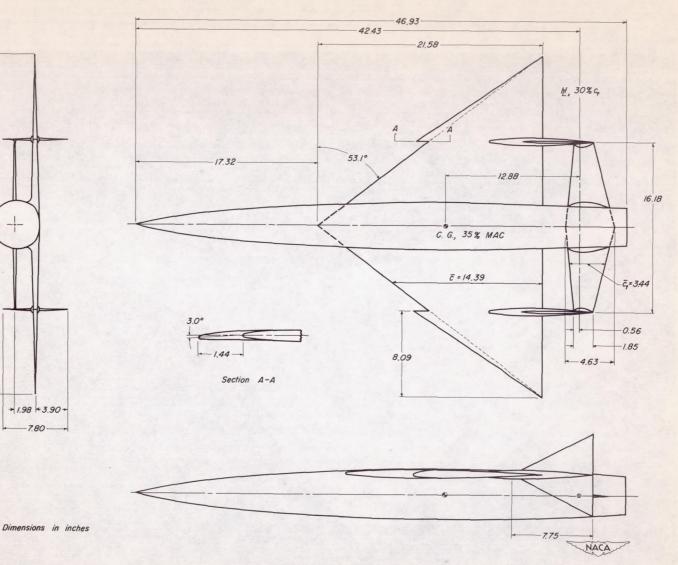


Figure 1. - Dimensional sketch of the model.

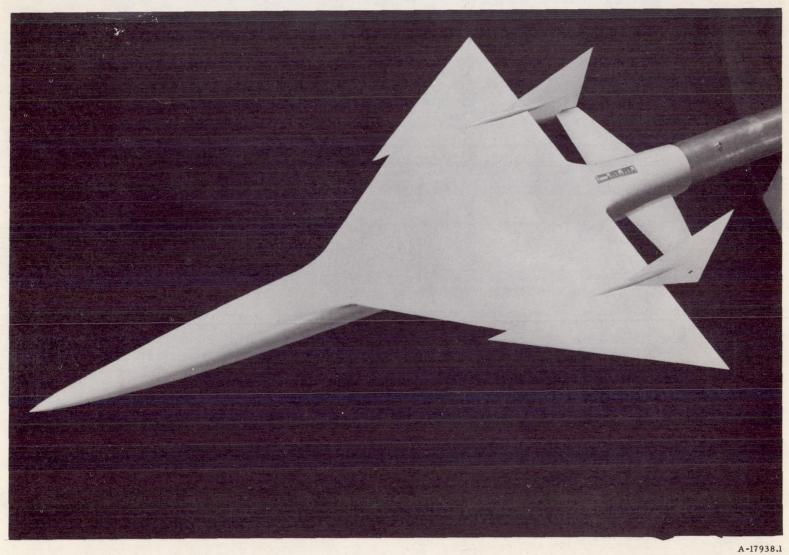


Figure 2.- Three-quarter front view of wing-body-tail combination with leading-edge chord extensions.



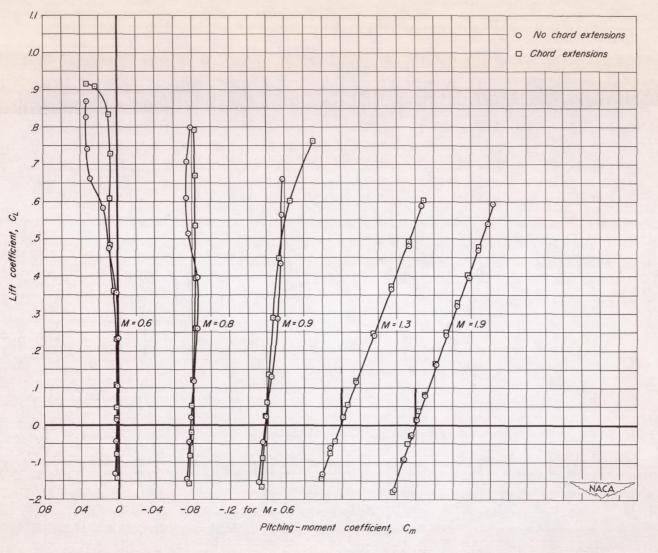


Figure 3.- Effect of leading-edge chord extensions on the variation of pitching-moment coefficient with lift coefficient for a wing-body combination employing a triangular wing of aspect ratio 3 (vertical fins attached to wing).

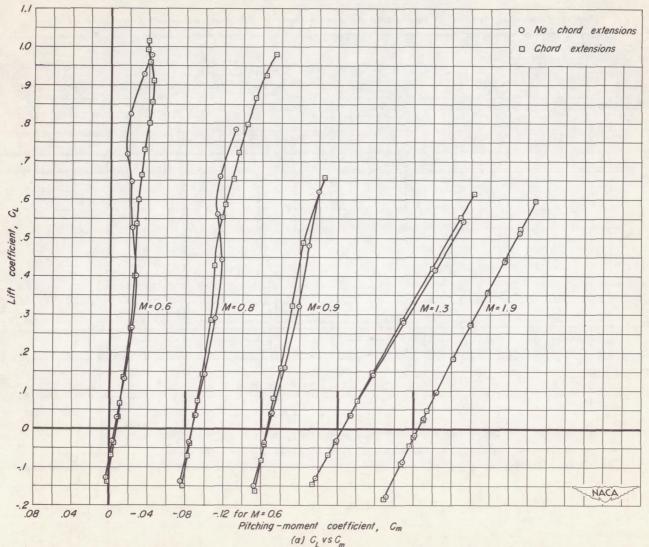


Figure 4.- Effect of leading-edge chord extensions on the aerodynamic characteristics of a wing-body-tail combination employing a triangular wing of aspect ratio 3 and an all-movable horizontal tail,  $\delta_n$ =0.

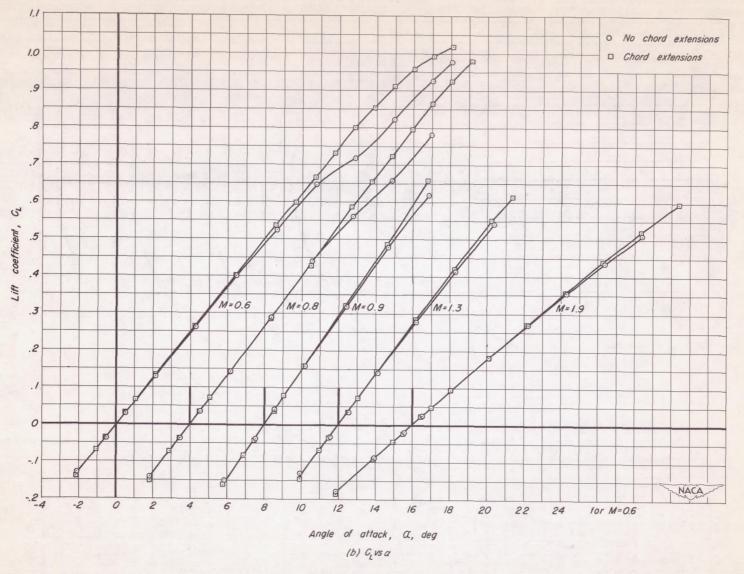


Figure 4. - Continued.

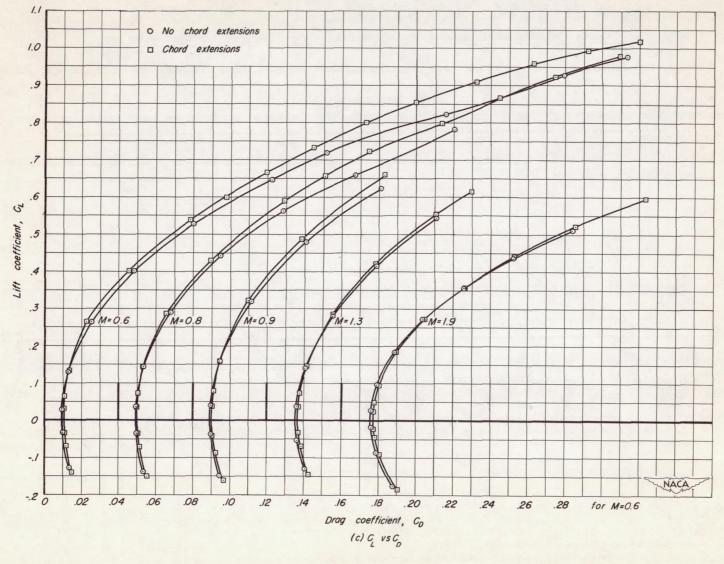


Figure 4. - Concluded.

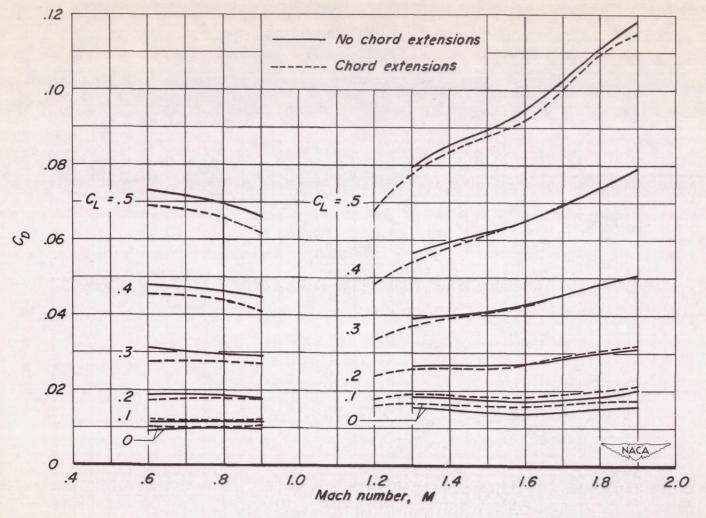


Figure 5.— Effect of leading—edge chord extensions on the variation of the drag coefficient with Mach number for the wing—body—tail combination,  $\delta_n = 0$ .

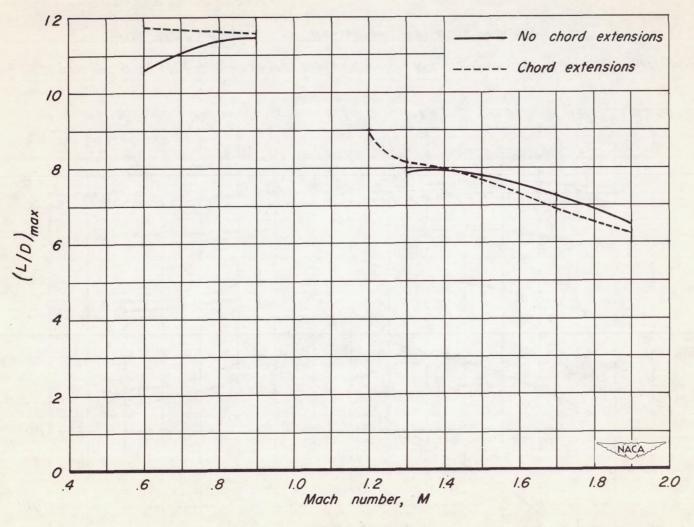


Figure 6.— Effect of leading-edge chord extensions on the variation of the maximum lift-drag ratio with Mach number for the wing-body-tail combination,  $\delta_n = 0$ .

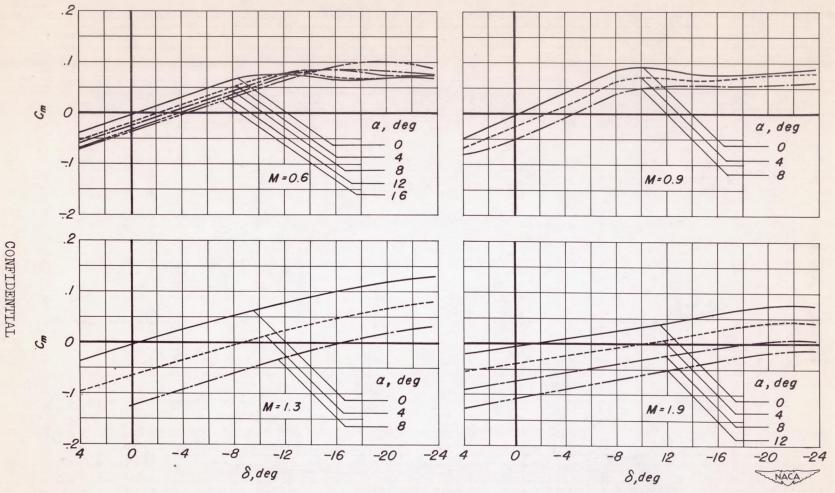


Figure 7.- Variation of the pitching-moment coefficient with horizontal-tail deflection for the wing-body-tail combination with leading-edge chord extensions.

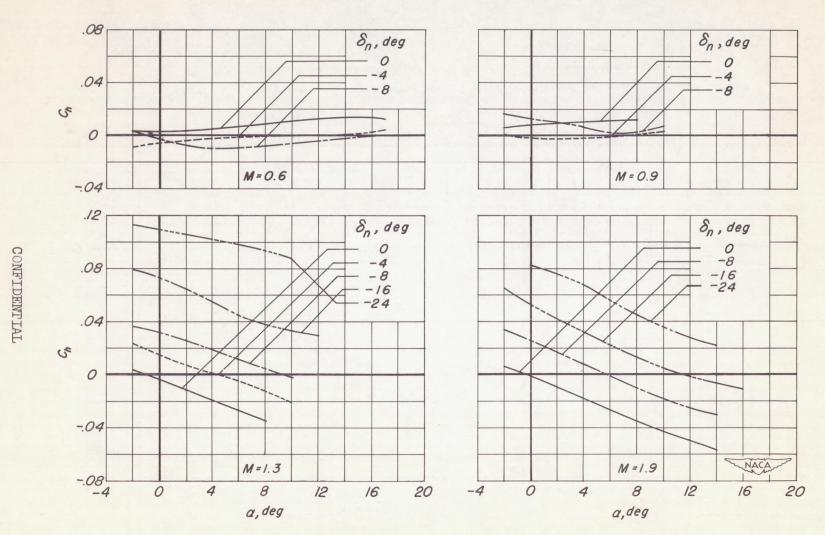


Figure 8. - Variation of the horizontal-tail hinge-moment coefficient with angle of attack for the wing-body-tail combination with leading-edge chord extensions.

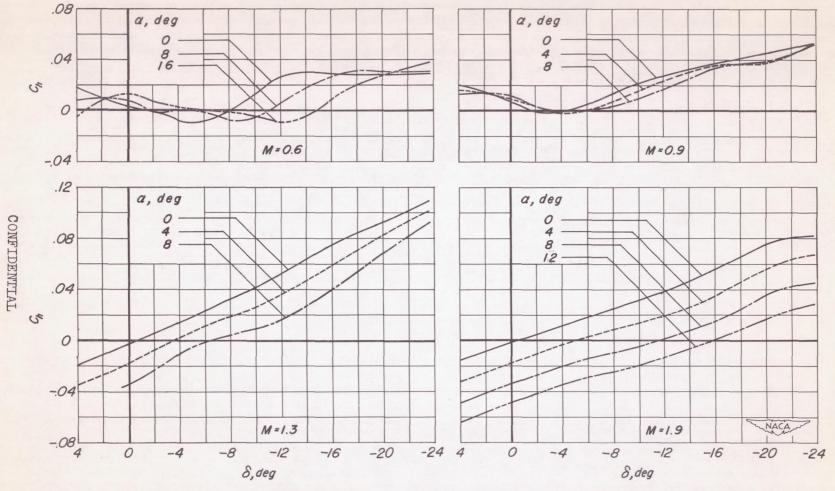


Figure 9.- Variations of the horizontal-tail hinge-moment coefficient with angle of deflection for the wing-body-tail combination with leading-edge chord extensions.

